

Inter Office Memo



Consumer Electronics Division

To: ATTENDEES

From: A. Leon *A.L.*

Subject: NEW SELF-CENTERING ANALOG CONTROLLER KICK OFF
MEETING

Date: 4/13/83

S. Upjohn of domestic marketing generated a summary Product Requirement Statement for 5100/5200 New Controller. This meeting was called to discuss engineering's position to design, develop the requested new controller within the limits specified by marketing.

The meeting started at 10:15 A.M. The attendees were:

C. Asher
A. Leon
B. Mizerek
D. Kramer
J. Jessep
M. Biasotti
A. DeSchweinitz
S. Upjohn

SUMMARY OF MEETING

1. Approaches

3 Approaches were identified.

- A. With present tooling, aim for improved cost performance ratio.
- B. With new design (new tooling) aim for low cost high reliability and high performance.
- C. Total new radical design (pistal grip etc.....).

2. Cost

The cost limitation of \$3.50 each is thought to be possible with approaches A and B. However, C. Asher felt the pistal grip will cost more than the \$3.50/each limit.

Discussion on the cable cost indicated that cables made in U.S. costs around \$3.00 each whereas cables made in Taiwan cost around \$1.50.

3. Schedule

1. If the design requires new tooling, an estimated "production tool ready" time is = FEB 1984. This is not acceptable to Marketing.
2. A. DeSchweinitz will assist and look into internal soft tool capabilities.

Schedule (cont.)

3. If approach A is used, then target ship date of Dec. 1983 requested by marketing is possible.

4. Marketing Technical Requirements

In the course of design, marketing requests that engineering should look into the following:

1. More tactile feed on the fire button.

2. No rubber boot.

3. Ergonomics as much as possible (human Engineering).

4. If time is available, investigate the following:

a. gating alternatives.

b. on/off self centering selection.

5. Frame design should be flexible to include future digital 3600.

5. Engineering Position

1. M. Biasotti and C. Asher have agreed to get together and generate an analysis of the 3 approaches identified in section 1. Analysis will include schedule, cost and what's involved.

2. This analysis will be distributed to the attendees on May 4, 1983.

3. Follow up meeting is scheduled for Friday May 6, 1983. A. Leon will sent out meeting notice.

The meeting adjourned at 11:15 A.M.

AL/1b

cc: K. Ashton
R. Nishi
D. Remson
G. Blondefield
B. Goldberg

PRODUCT REQUIREMENT STATEMENT

5200 CONTROLLER

GENERAL

NEW SELF-CENTERING

Name: Low-Cost 5200 Controller

Top Assy Number: TBD

Target Cost: Under \$3.50 each [REALISTIC, BUT ASSEMBLED IN HI-COST U. S.]
(materials only)

Target Ship Date: December, 1983 [FEB '84 FOR NU DESIGN]

MARKETING RATIONALE

Current controller presents the following problems:

- low reliability (boots and fire buttons)
- inadequate fire buttons
- high cost
- not enuff fun to play

TECHNICAL REQUIREMENTS

- self-centering analog design*
- compatible with all 5200 products
- for hand-held use
- no single source parts
- -- increased tactile feedback on firebuttons*
- ? -- no rubber boot*
- -- ergonomic redesign of fire buttons and controller housing
 - selective on-off self-centering

ALFRED
ASH PLOT
"PATENTS IN PROGRESS"

OTHER

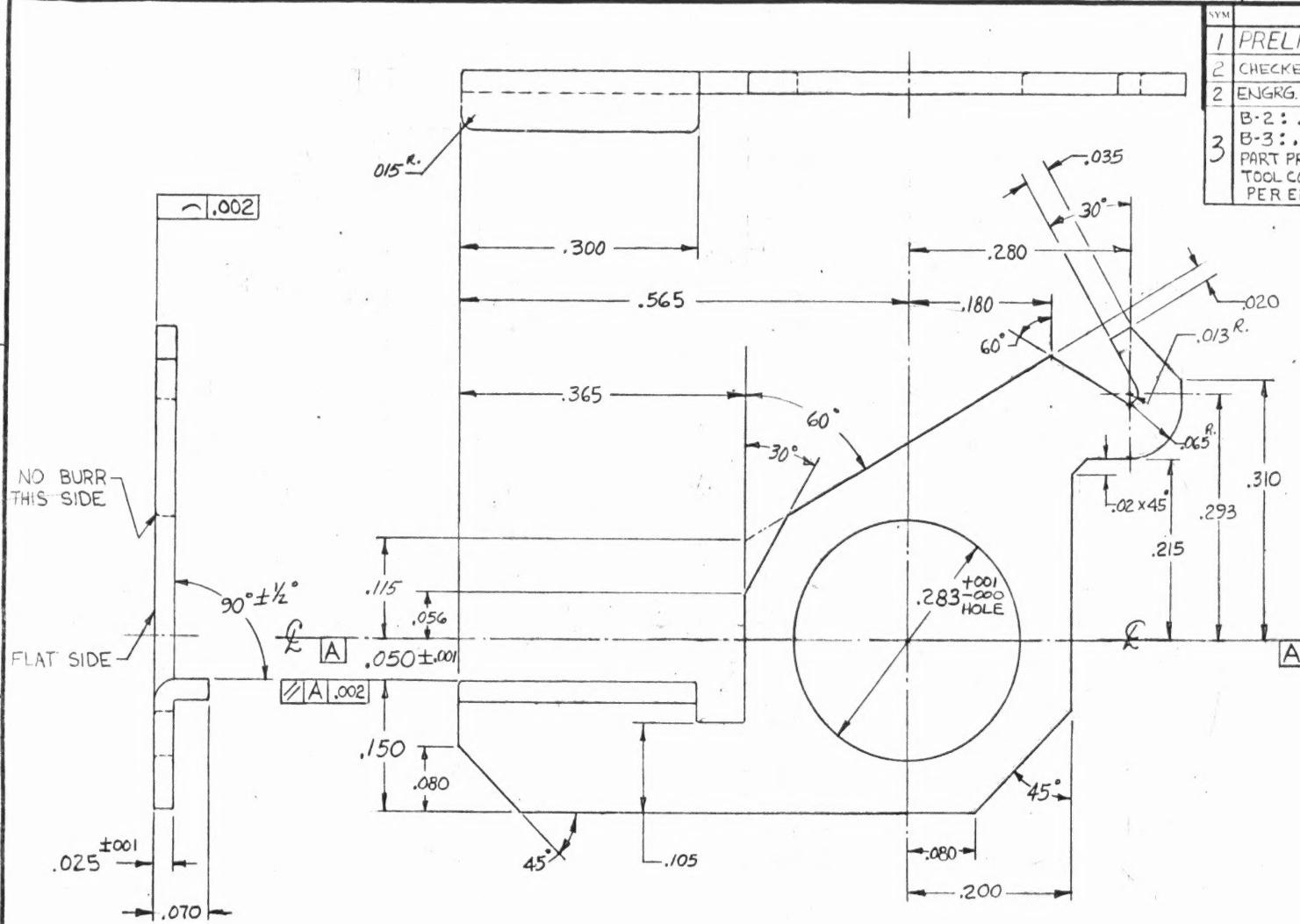
- investigate gating alternatives*

- '3600 digital-analog controllers'

NEW MTG FRI. MAY 6, 10:30

UPSTAIRS CONF. ROOM

SYM	REVISIONS DESCRIPTION	DATE	APPROVED
1	PRELIMINARY RELEASE	7/13/83	
2	CHECKED RELEASE	7/17/83	
2	ENGRG. REL, ERC # E0116A	6-10-83	PA8
3	B-2 : .283 $\pm .001$ WAS .283 $\pm .002$ B-3 : .050 $\pm .001$ WAS .050 $\pm .002$ PART PROFILE CHANGED FOR EASIER TOOL CONSTRUCTION & MAINTAINANCE PER ERC E0174	7-13-83	Xa
		7/18/83	PA



ENGINEERING
RELEASED

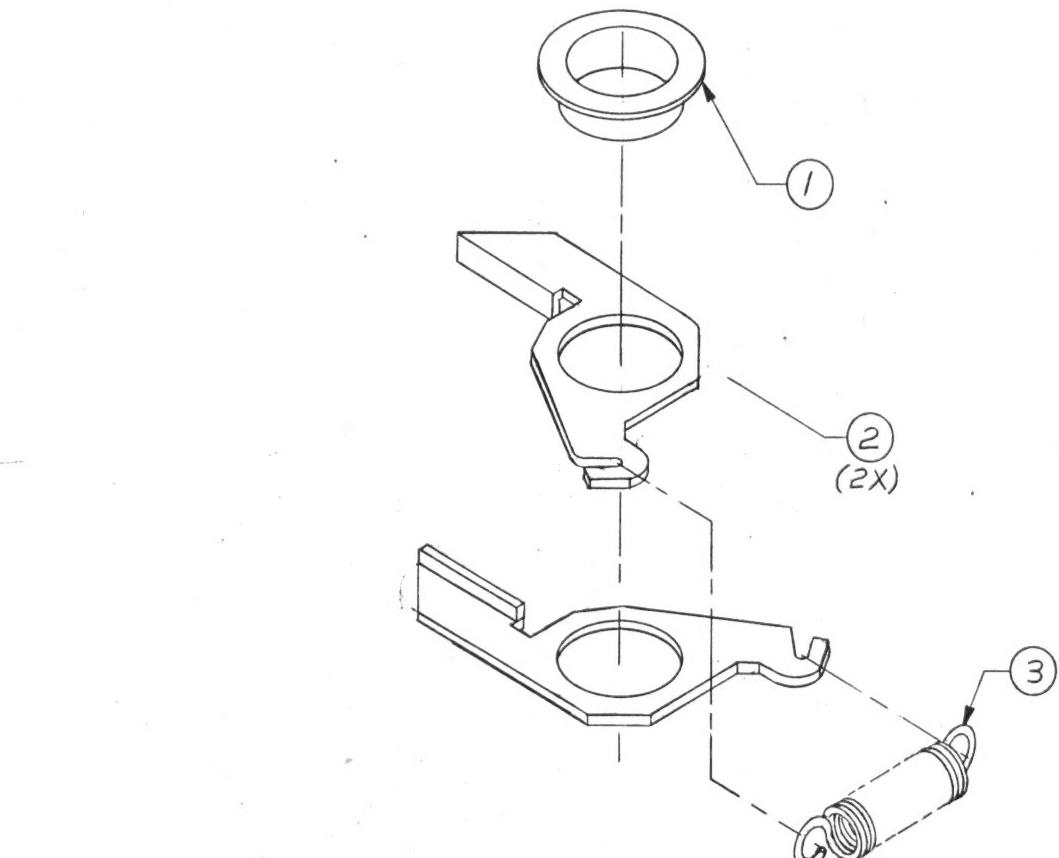
CA022057	CX-52	UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ON: ANGLES = ±1° SURFACE FINISH ✓	DRAWN BY <i>J. Craig Acheson</i> DATE 5-17-83
NEXT ASSY	USED ON	x = ±.1 xx = ±.01 xxx = ±.005	CHECKED M. D. Allen DATE 5-17-83
APPLICATION		MATERIAL: .025" CRS. (SOFT) TUMBLE DEBURR	ENGINEERED BY <i>J. Craig Acheson</i> DATE 5-18-83
		FINISH: 50 MICRO/IN. ELECTROLESS NICKLE PLATE	ENGINEERING MGR. <i>K. Acheson</i> DATE 5-18-83
		QUALITY ASSURANCE	
		MFG. ENGINEERING	
SIZE C		DRAWING NO. CO22058	REV 3
SCALE 10 : 1		SHEET 1 OF 1	

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1272 Borregas Avenue
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ATARI® A Warner Communications Company

TITLE: ARM, SELF CENTERING

4	3	2	1
SYM	REVISIONS DESCRIPTION	DATE	APPROVED
1	ENRG REL ,ERC # EO116A	6/10/83	CAG
2	REV PER ERC EO174	7/18/83	JHR



.105
MAX

ROLL OVER

.010
GAP

ASSY DETAIL

CAO18988
NEXT ASSY
APP

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3	1	CO22060	SPRING, EXT
2	2	CO22058	ARM, SELF CENTERING
1	1	CO22059	BUSHING
ITEM	QTY	PART NUMBER	DESCRIPTION
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ON: ANGLES: $\pm 1^\circ$ $x = \pm .1$ $xx = \pm .03$ SURFACE FINISH ✓ $xxx = \pm .005$			
<p>DRAWN BY <u>Don Falkenberg</u> DATE <u>5/13/83</u></p> <p>CHECKED <u>J.C.L.</u> DATE <u>5-18-83</u></p> <p>ENGINEERED <u>J. Coughlin</u> DATE <u>5-18-83</u></p> <p>ENGINEERING MGR. <u>K. Achelis</u> DATE <u>5-18-83</u></p>			
<p>MATERIAL:</p> <p>FINISH:</p>			
<p>QUALITY ASSURANCE DATE</p> <p>MFG. ENGINEERING DATE</p>			
SCALE <u>4X</u>		SHEET <u>1</u> OF <u>1</u>	REV <u>2</u>

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Sunnyvale, Calif. 94086

The Atari logo, featuring a stylized 'A' shape above the word "ATARI".

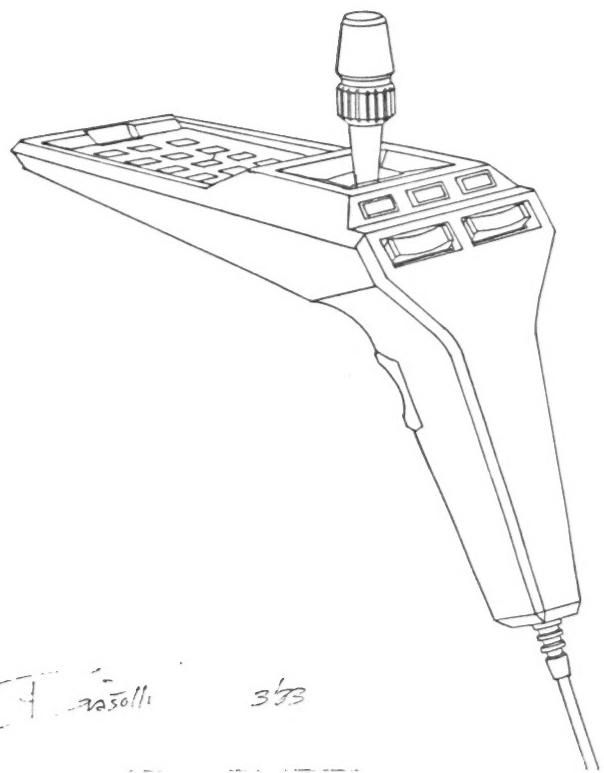
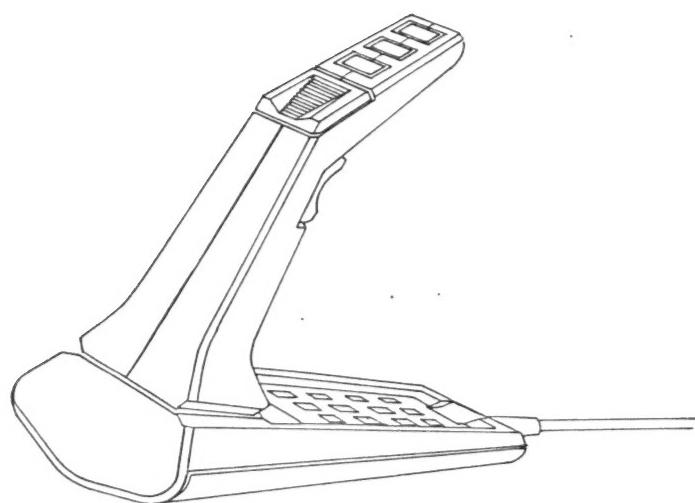
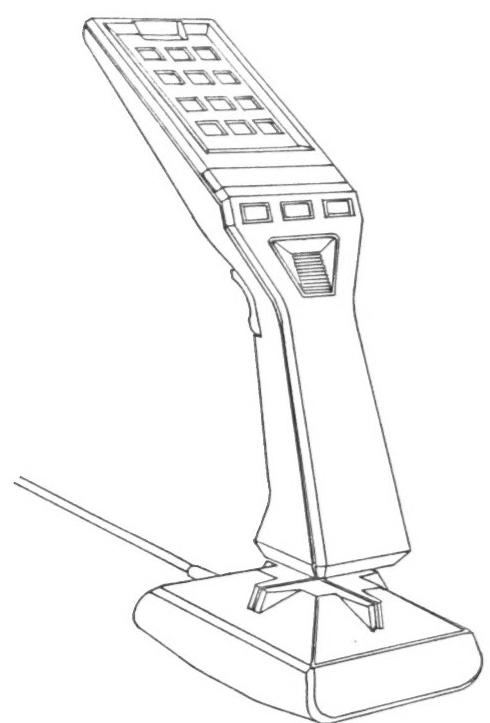
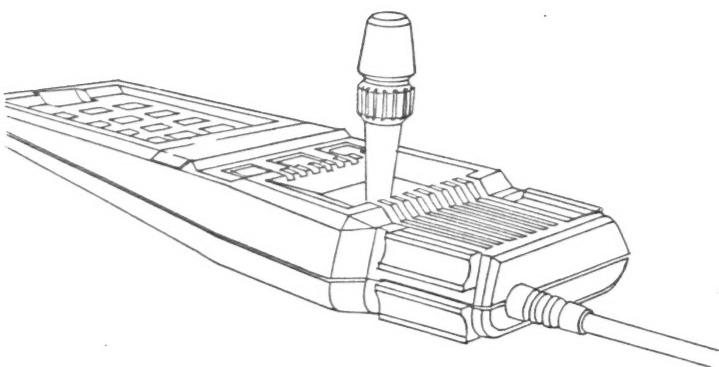
TLE

SELF CENTERING
ARM ASSY

DRAWING NO.
CA022057

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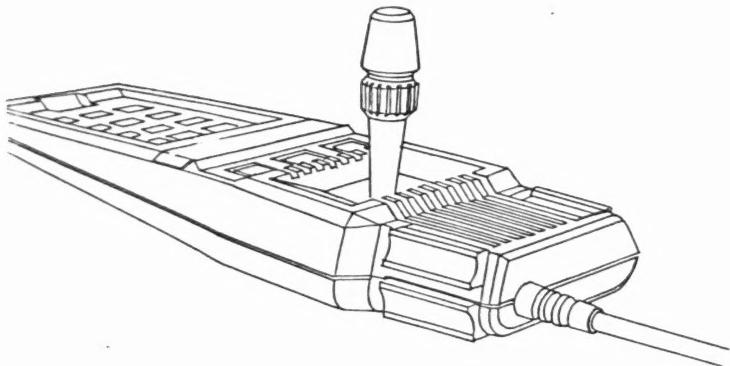
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F. Basoli

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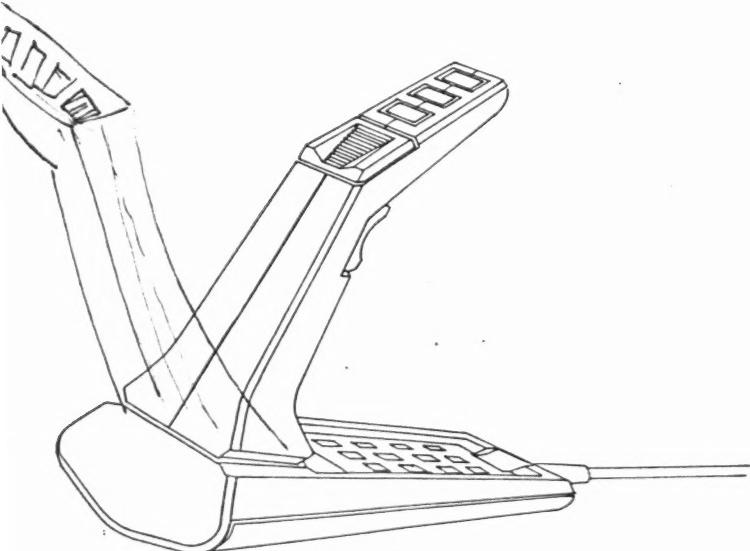
MORE OF THE SAME, BUT FIRE BUTTONS BEING RECESSED COULD CAUSE MORE FATIGUE.

DIGITAL
EXCESSIVE LEVERAGE, WI TOO-SMALL BA
NEEDS SMALLER- AND LARGER BOTTOM FOR BETTER GRIP.



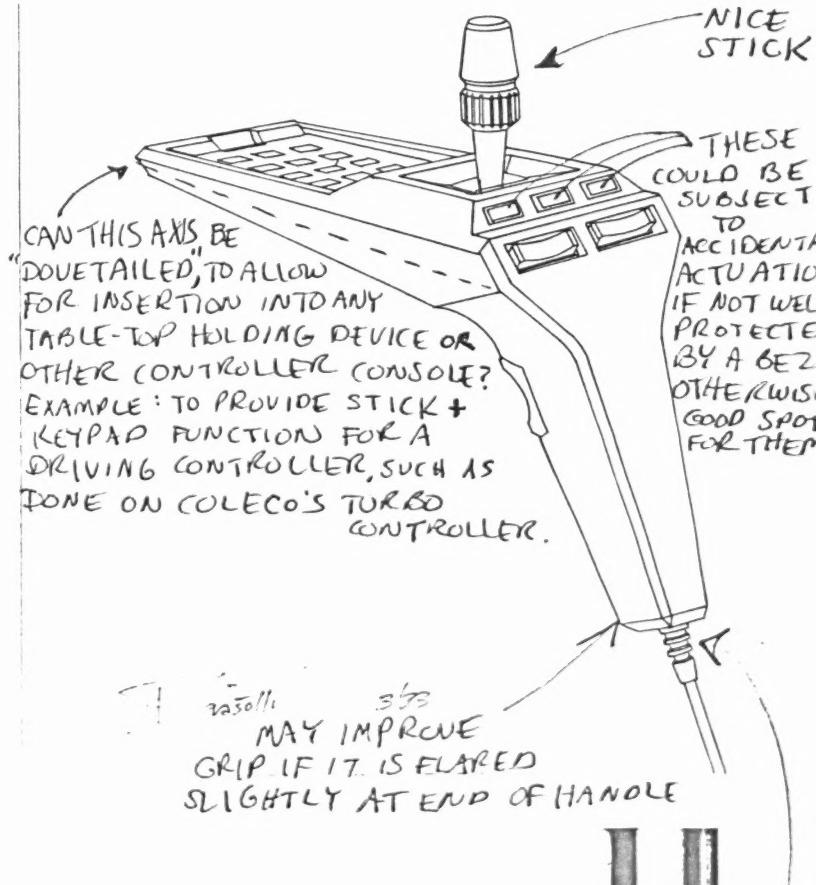
GOOD CONCEPT, THOUGH!

MIXMASTER DEELUX



HANDLE SEEMS TO BE TURNED THE OPPOSITE DIRECTION FOR EASY COMFORT GRIP

ANALOG - YEAH!



raselli 3/3
MAY IMPROVE GRIP IF IT IS FLARED SLIGHTLY AT END OF HANDLE

November 22, 1983

TO: Tom Kennedy

FROM: J.Jessop/E.Breeze/A.Tanaka

RE: 5200 ENHANCEMENTS/PRIORITIES

1. Hand Controllers

Present design needs thorough review.

- a. Lower cost with easier manufacturability and serviceability.
- b. Reliability needs to be improved dramatically. Warranty repair cost is a major drain on the company.
- c. Subjectively the game playability leaves a lot to be desired.
- d. Preferably a new design should be implemented to counter the negative consumer perception of the present design.

2. CONSOLE DESIGN

- a. Reduce the cable clutter, i.e. pluggable power module, IR link, loop through antenna connection and power.
- b. Front load console similar to front load VTR. This allows the unit to be stackable with other audio-visual equipment, so the customer will be deterred from storing the unit in closet/attic.

3. GAME ENHANCEMENTS

- a. Integrate the 2600 game cartridge compatibility and make the game ports adaptable for 2600 use.
- b. With the 2600 compatibility, the unit can play advanced games as proposed for the TIA SQUARED project.
- c. Investigate the feasibility of using faster system clock to increase overall performance.
- d. Improved expansion capability to accomodate video disk, optical ROM, and other peripherals similar to COLECO.
- e. Two player stereo headphone jack. Independent channel capability for the present and new generation games. This will allow the sounds and instructions to be audible to each player independent of each other. This has exciting possibilities for strategic action type games.
- f. System power down feature to resume former play after interruption. Useful in long playtime games such as chess and adventure games.

CC: D. Teiser
C. Goy

ENGINEERING RELEASED DISTRIBUTION LIST

PROJECT TITLE: ANALOG CONTROLLER		MODEL NO:		DIST CODE:	L
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ENGINEERING RELEASED

PROJECT NAME

MODEL

PROJECT MANAGER

ANALOG Controller

cx5R

HANS KRAMER

L

PART NUMBER

REV.

DESCRIPTION

ECN NO.

DATE
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CA022057

2

ARM ASSY

80174

7/22/83

CD22058

3

ARM

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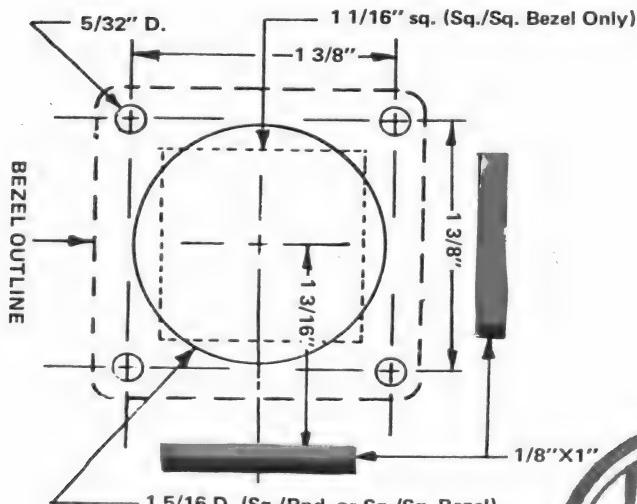
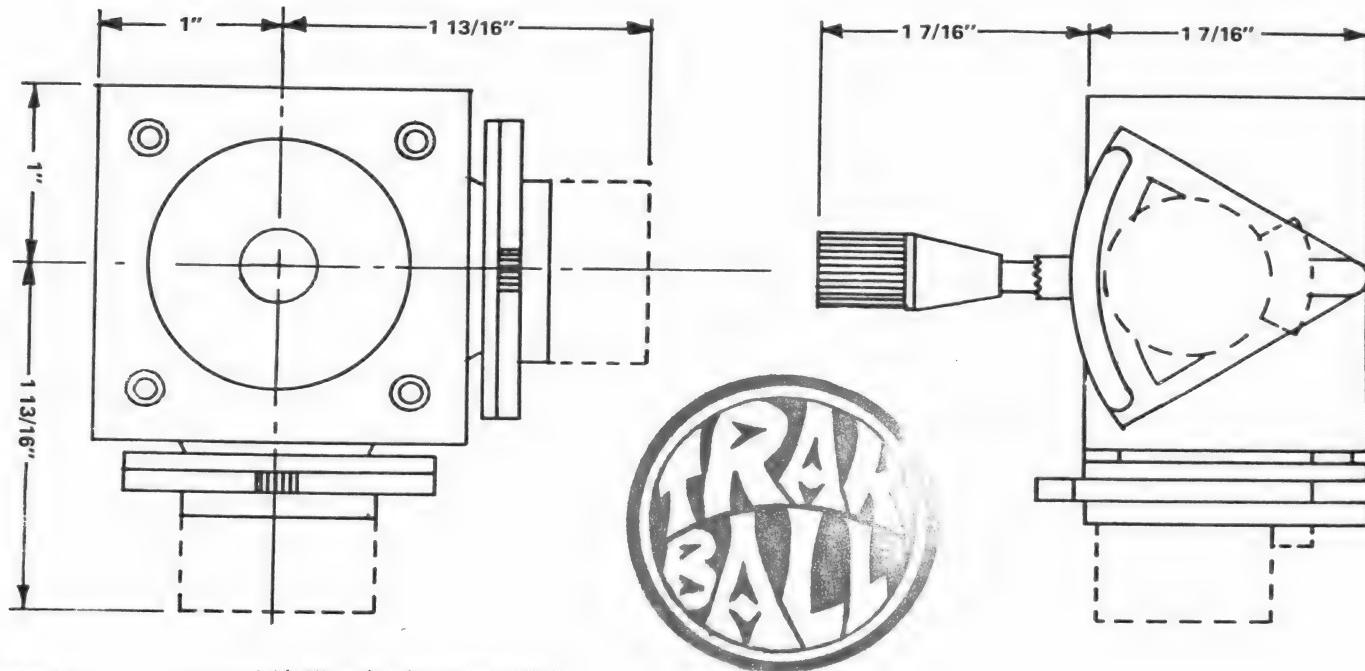
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THE MKII CONTROL GIMBAL

DESCRIPTION

The MK II stick is a top quality, precision molded, two axis control gimbal intended for applications such as game joysticks, computer plotters, remote control transmitters and controllers, or any other uses requiring infinitely variable potentiometer settings in two axis. Both functions can be either self-centering or not and have a fine centering trim adjustment which is externally accessible. The trims don't have to exist if desired. Two styles of bezels are available; one with a square inner area, the other with a round inside.

The stick features quick assembly, smooth and accurate operation, very easy calibration, rugged design and long life. Also it is significantly less expensive than most alternatives that are available today.



FACEPLATE CUTOUT REQUIREMENTS
(material thickness .050-.125")

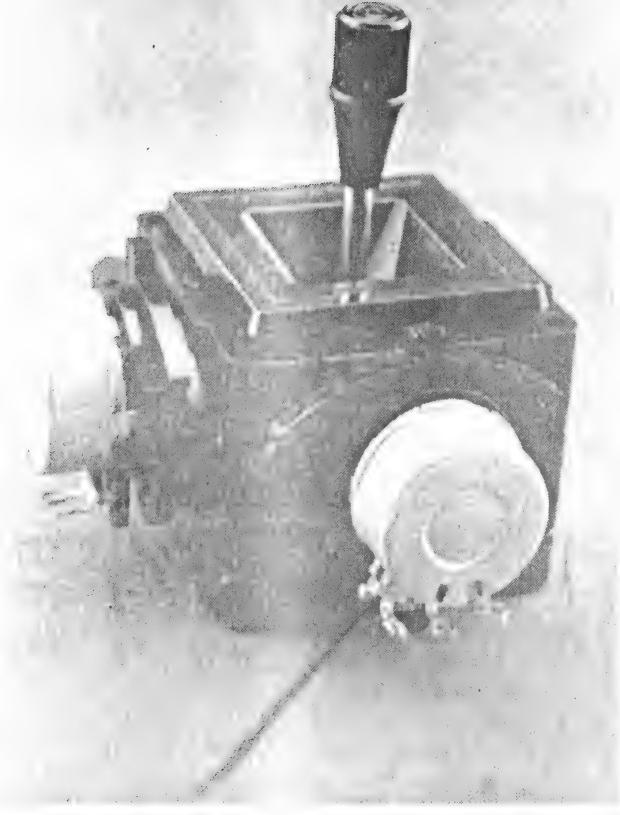
POT SPECIFICATIONS

Any diameter pot with a 3/8-32 UNEF - 2A standard threaded bushing and a 1/4" X 3/8" shaft will work. The distance between the mounting face of the pot and the end of the shaft should be .812" \pm .015".



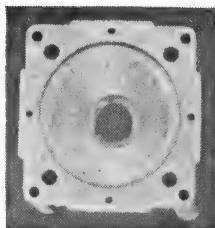
ACE R/C, Inc.

BOX 511 116 W. 19TH ST. HIGGINSVILLE, MO. 64037



ACE R/C, Inc.

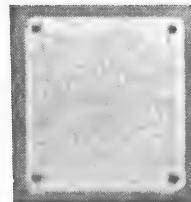
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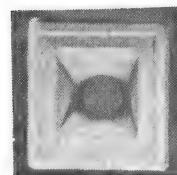
15E72—Front Housing Box



15E78—Ball Retainer



15E73—Gimbal Box Lid

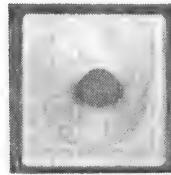


15E83—Stick/Ball Assembly

(OR)



15E84—Spring Return Lever



15E70—Square/Square Face Cup



15E82—Large Bale



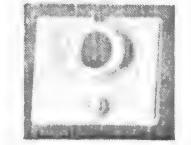
15E81—Small Bale



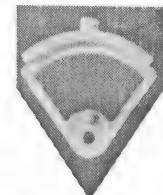
15E80—Bale Retainer Side Plate



15E94—Spring



15E79—Pot Side Plate

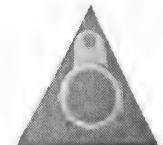


15E74—Trim Lever

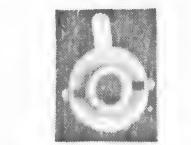
(OR)



15E93—Pot Nut



15E76—Friction Ring

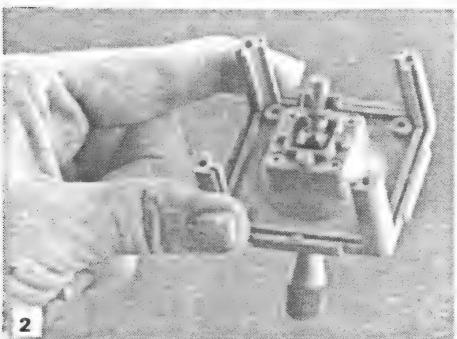


15E77—Pot Lock Ring

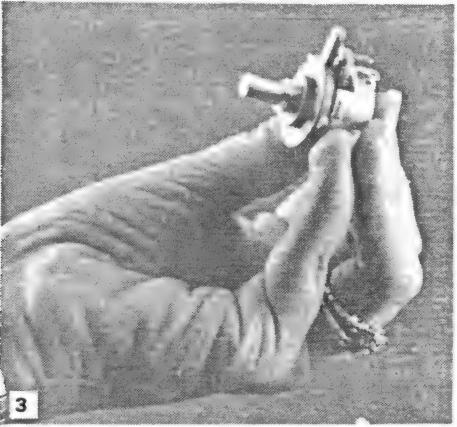
15E75—Trim Lever Substitute



1—Insert Stick/Ball Assembly at an angle to clear Ball Retainer.



2—Tighten Ball Retainer screws until stick still moves when the Housing Box is jiggled.



3—Note orientation of parts.



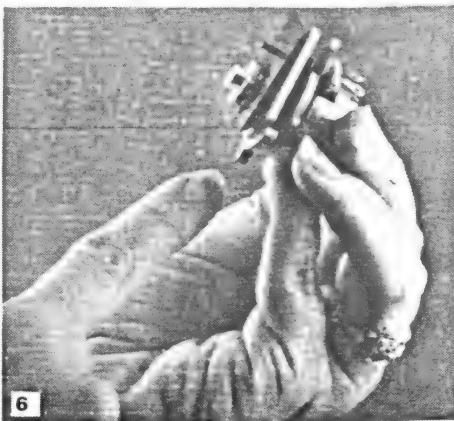
4—Make sure flat sides of Pot Lock Ring and Friction Ring are towards pot.

ACE MK II STICK ASSEMBLY

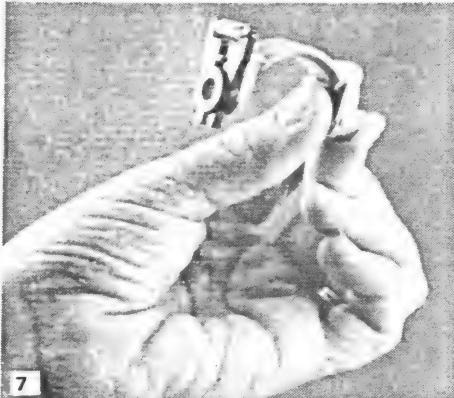
This is not step by step instructions, but a photo sequence to aid in assembly. The use of gray and black parts is for visual clarity.



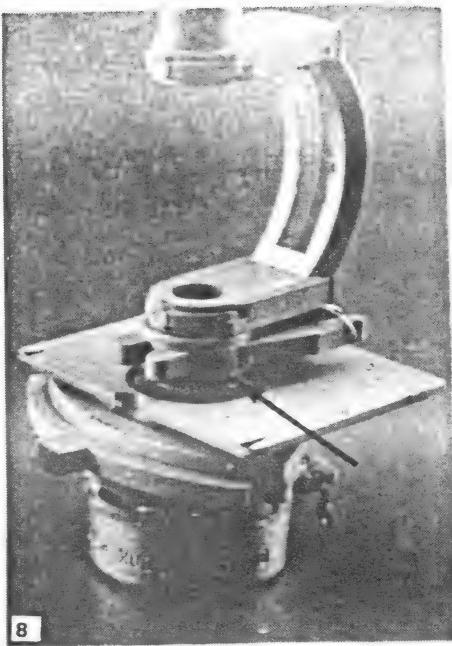
5—Button, on Trim Lever, faces out to engage mating hole in Friction Ring. NOTE If Trim Levers are not used, insert Trim Lever Substitute.



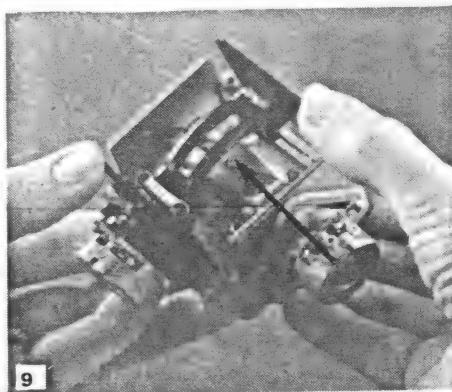
6—Center Trim Lever.



7—Spring Return Levers and Spring are centered on Bale.

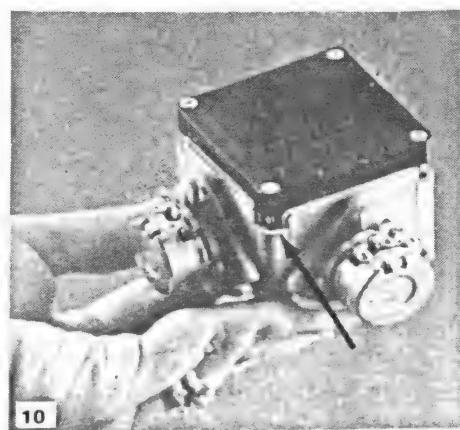


8—There must be .005" to .007" clearance between Spring Return Levers and Pot Nut.



9—Install Small Bale Assembly, then Large Bale Assembly into Housing Box. Make sure Stick end piece goes through each Bale.

NOTE: Before the Gimbal Box Lid can be put on the Face Cup and assembled Gimbal must be fastened to panel using four 2-56 x 1/4" pan head screws.



10—Install Gimbal Box Lid with four 2-56 x 1/2" F.H. screws. Allow .010" gap at corner posts.

ACE R/C, Inc.

BOX 511 HIGGINSVILLE, MO. 64037 816 584-7121



ENGINEERING LOG SHEET

2

11/29/82

GAME OR PROJECT

Spectravision Joystick Analysis

Spectravision Joystick Model 318-101

Electrical:

$$\text{RESISTANCE} = \Omega$$

1) Contact Resistance

- A) Pin 1 = UP Position 5Ω to 8Ω
- B) Pin 2 = Down Position 15Ω to 98Ω
- C) Pin 3 = Left Position 7Ω to 40Ω
- D) Pin 4 = Right Position 5Ω to 38Ω

2) Contact Bounce MEASURED AT FIRE Button was found to be 1v for 5ms



3) PCB Consisted of ONE Board with contact switches mounted on it.

4) Assembly was quite EASY AS well AS disASSEMBLY

Game Application

- 1) HUMAN ENGINEERING ~~was~~ should be given 90%
 - 2) EASE of ACTUATION is A 80% due to the lack of Centering Ability
 - 3) Direct UP-DN-Rt-Lt MOTION is A 95%
 - 4) DIAGONAL MOTION is A 75% Has a tendency to want to go Rt or Up
 - 5) FIRE button is comparable to Atari
- ** OVERALL due to the Human Engineering Concepts I would have to RATE this joystick a 80%

SUBJECT: A PIEZOCERAMIC BENDER CONTORLLER

A piezoceramic bender controller could be produced using a square shaft with piezoceramic wafers laminate on all four sides. The direction would be detected by the voltage change of the two wafers on opposite sides of the shaft for each axis. If a third axis was needed for a product a curved piezocermic bender could be used which would be controlled by squeezing either a trigger button or squeezing the grip.

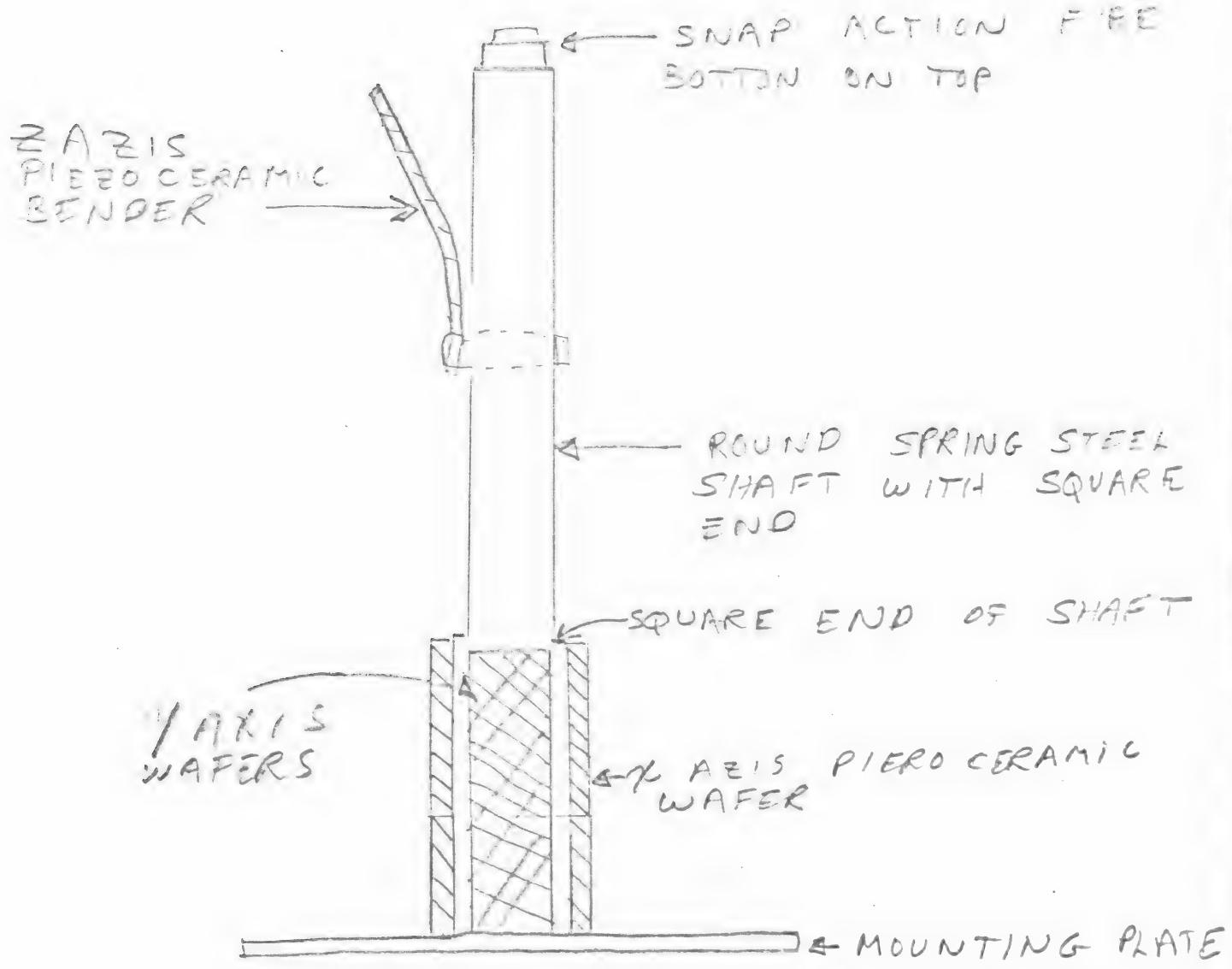
The controller would have very few moving parts. Spring steel would need to be used for the shafts. The controller could be design to be very tough due to the mat'l required and the lack of moving parts required. The controller by design would have a automatic return to center by the fact that the shaft is spring steel.

The cost of the piezo and shaft should be low when compare to other systems used now. The shaft maybe could be made out of aluminum for lower cost and less weight if aluminum could be found with the right spring.

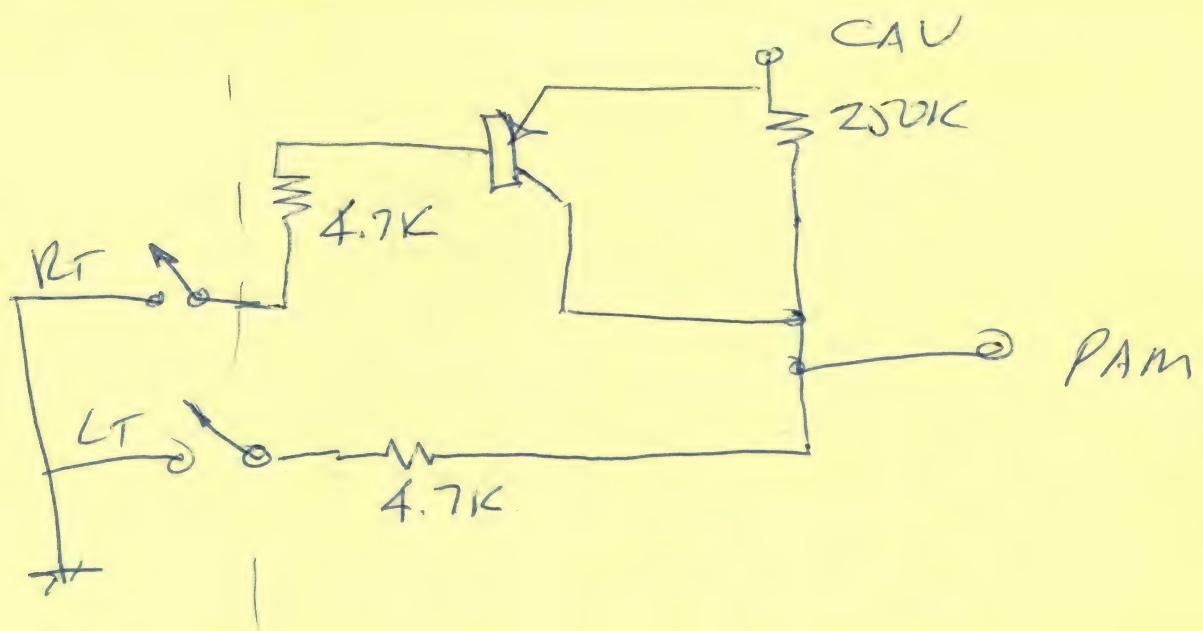
The firm of PIERO ELECTRIC PRODUCTS,INC of Cambridge Mass., Porter Stone : President, should be ready to lend a hand in design and production of a wafer-shaft compont.

Thank You

Rolan Denis Estrada



R D ESTRADA 8/19/e2



STICK
STICK - |
TO PAM
ADAPTER

PC CO18124

CABLE ASSY CAO 18145

SYM

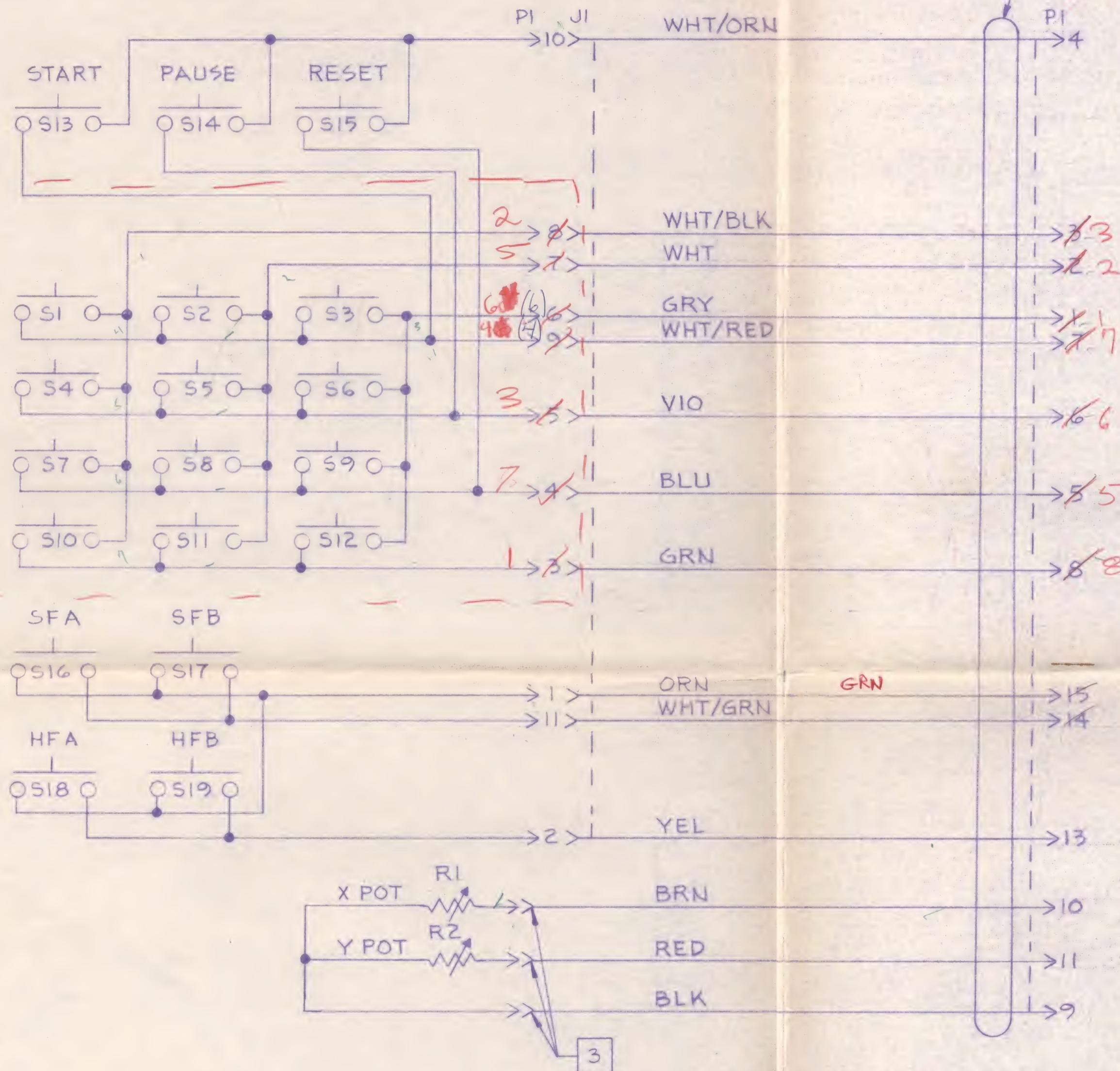
REVISIONS DESCRIPTION

DATE APPROVED

1

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3/29/82

D
KEY PAD P.C.B. ▶

NOTES:

1. FOR ASSEMBLY SEE CAO18107.
2. UNLESS OTHERWISE SPECIFIED:
SYMBOLS ARE PER ANSI STANDARDS.
- 3 SLIDE CONNECTORS.

JUL 13 1982
LATEST REVISION

OUTSTANDING ECNs

CAO18107	CX52
NEXT ASSY	USED ON
APPLICATION	

UNLESS OTHERWISE SPECIFIED
DIMENSIONS ARE IN INCHES
TOLERANCES ON:
ANGLES = $\pm 1^\circ$ x = ±
SURFACE FINISH ✓ xx = * xxx = *

DO NOT SCALE
DRAWINGDRAWN BY
FALKAR 12/4/81

MATERIAL:

CHECKED

ENGINEER
Peter Grimaldi 3/26/82PROJECT ENGINEER
3/20/82

MFG. ENGINEER

Atari, Inc.
1272 Borregas Avenue
Sunnyvale, Calif. 94086

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TITLE
SCHEMATIC DIAGRAM,
CONTROLLER
RAM CON

SIZE C DRAWING NO. CO18226 REV 1

SCALE — SHEET 1 OF 1

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DRAWING

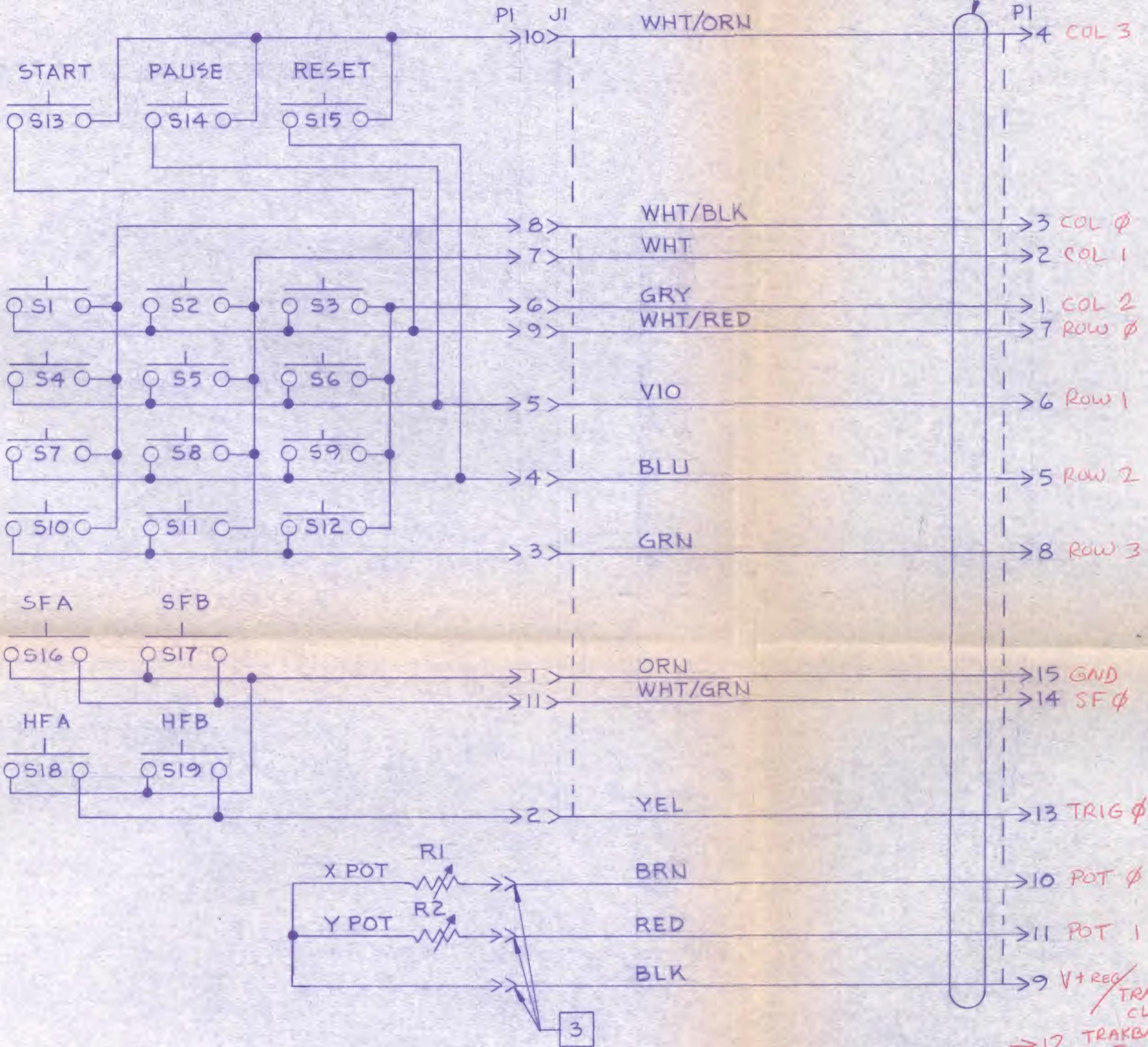
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3

PC CO18124

CABLE ASSY CAO18145



SYM	REVISIONS DESCRIPTION	DATE	APPROVED
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CO18226

SHEET 1 REV A

NOTES:

1. FOR ASSEMBLY SEE CAO18107.
2. UNLESS OTHERWISE SPECIFIED:
SYMBOLS ARE PER ANSI STANDARDS
3. SLIDE CONNECTORS.

OUTSTANDING ECNs

CAO18107	CX5200
NEXT ASSY	USED ON
APPLICATION	

UNLESS OTHERWISE SPECIFIED
DIMENSIONS ARE IN INCHES
TOLERANCES ON:
ANGLES = $\pm 1^\circ$ $x = \pm$
SURFACE FINISH ✓ $xx = \pm$
MATERIAL: $xxx = \pm$

DO NOT SCALE
DRAWINGDRAWN BY
FALKAR 12/4/81

DATE

CHECKED

ENGINEER
Peter Brown 3/26/82

PROJECT ENGINEER M. FALKAR

3/26/82

MFG. ENGINEER



Atari, Inc.
1272 Borregas Avenue
Sunnyvale, Calif. 94086

A Warner Communications Company

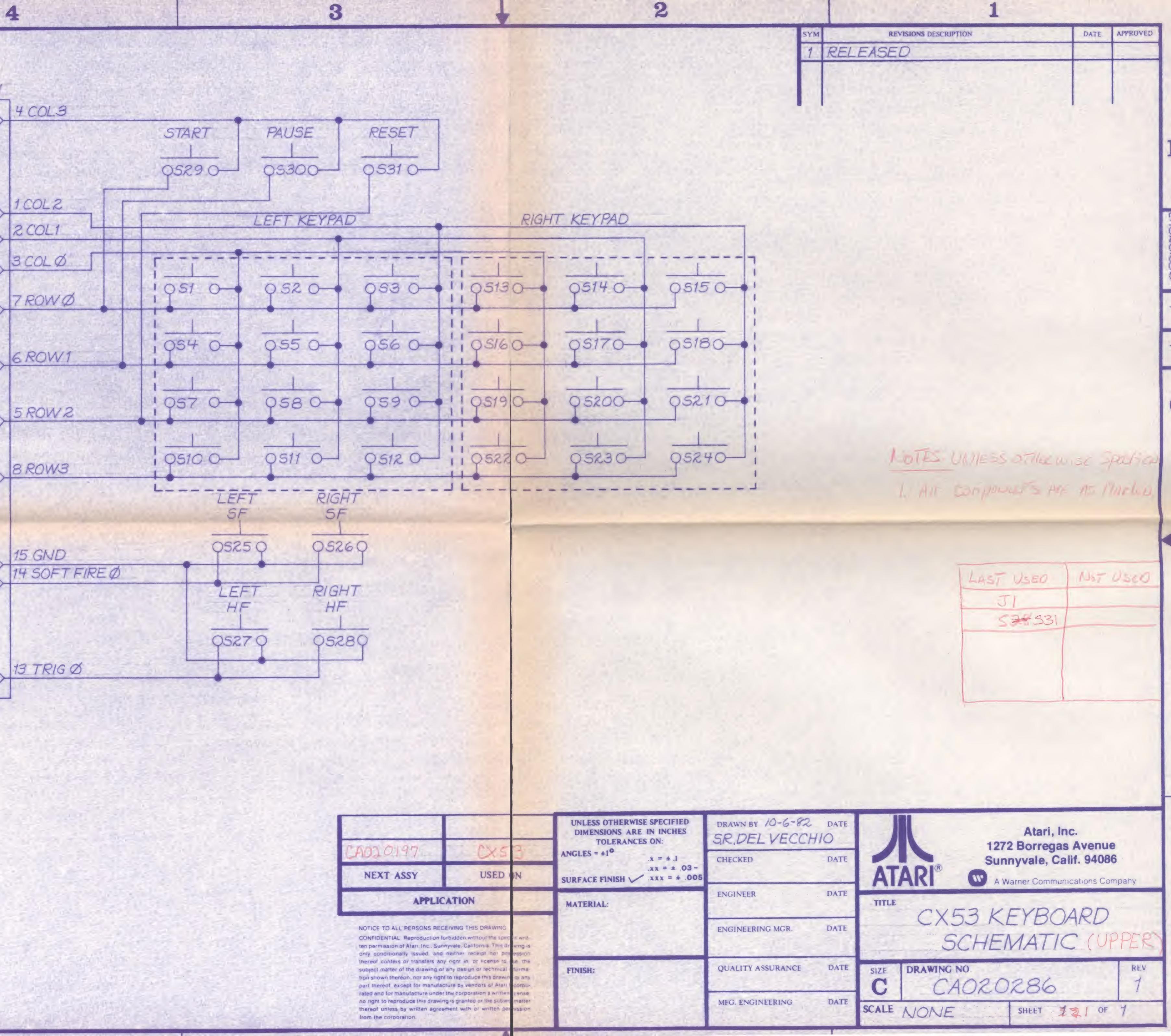
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CONTROLLER

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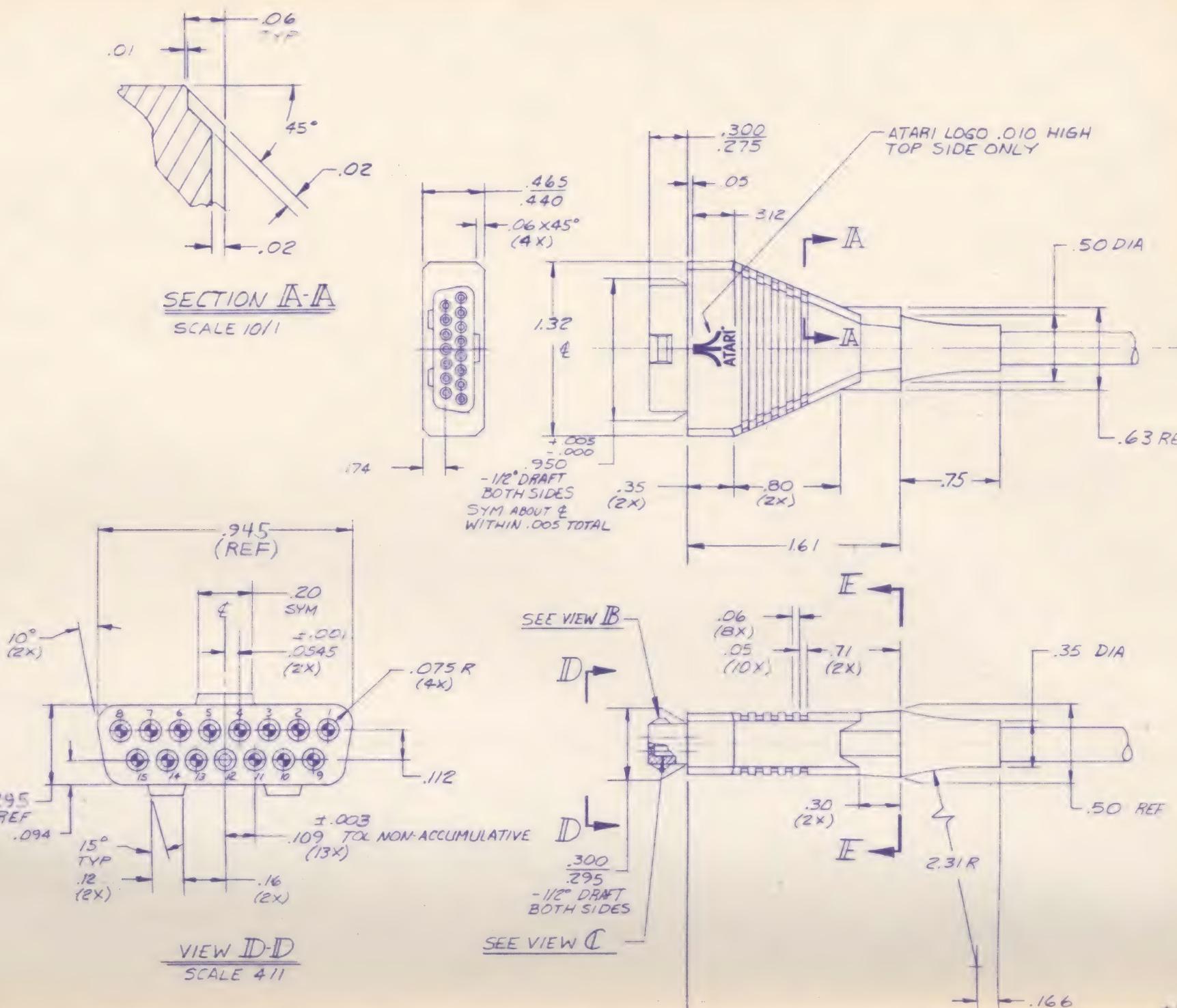
REV 1

NOTICE TO ALL PERSONS RECEIVING THIS
DRAWING

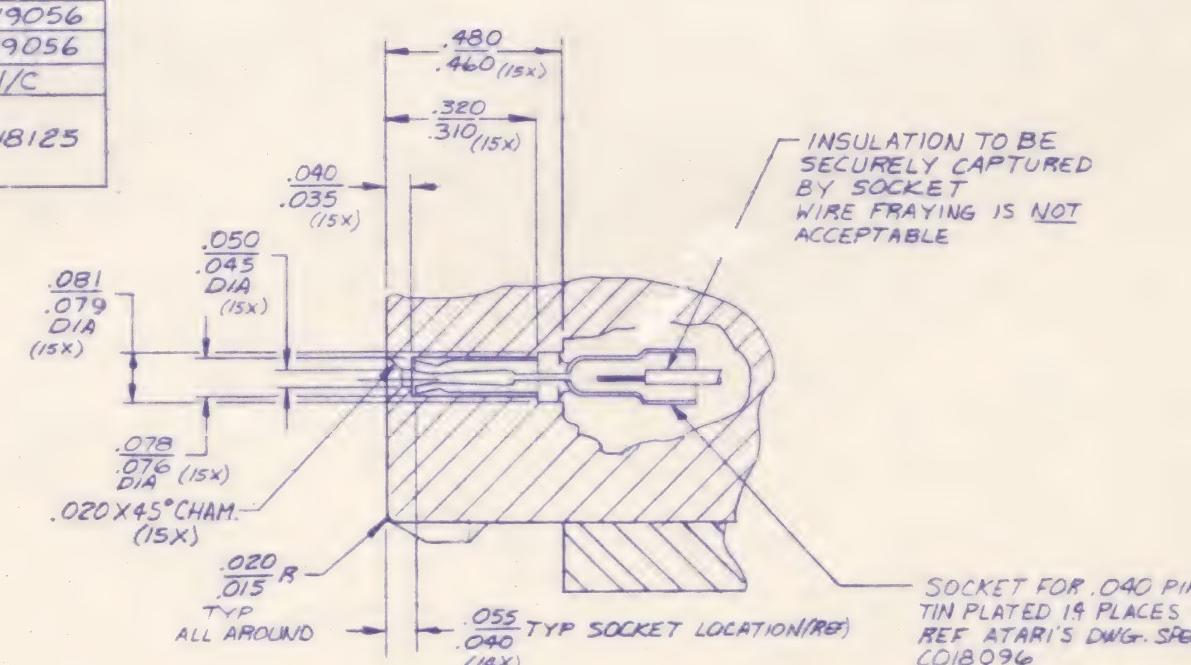
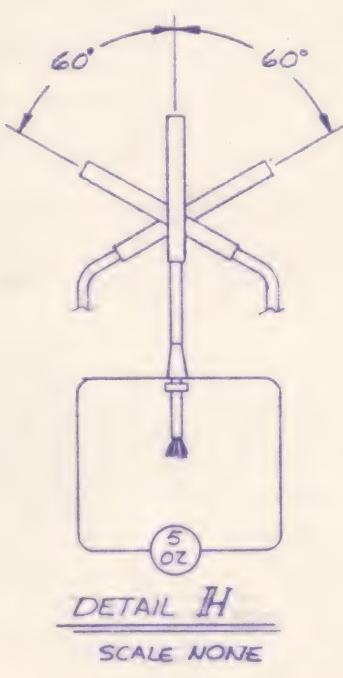
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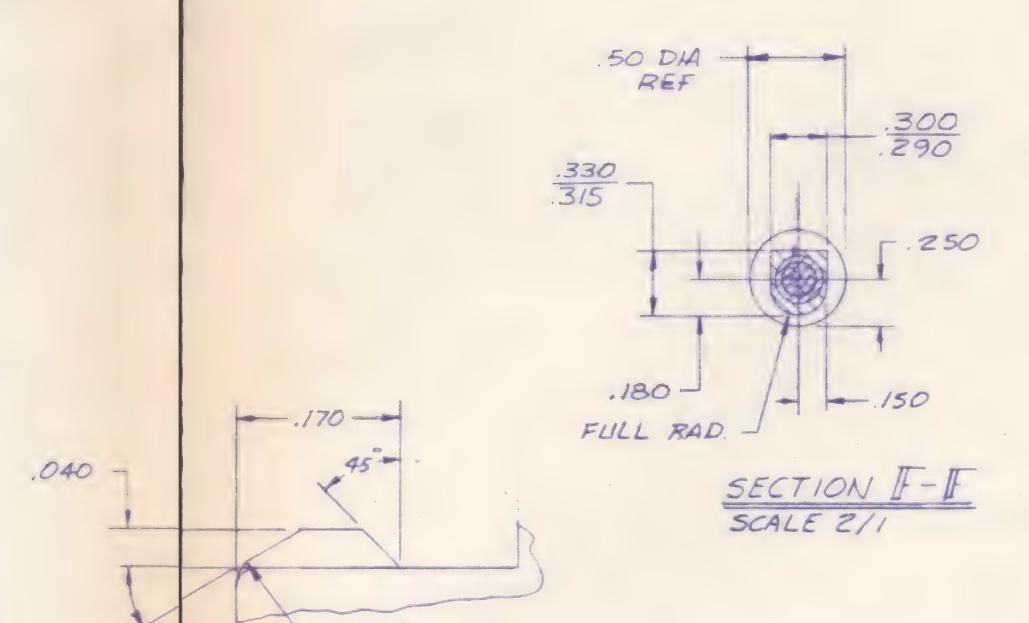
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REVISED & REDRAWN	1/10/81	
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REV. PER ECN 5361	4/28/82	Carj
REV. PER ECN 5478	6/4/82	Carj



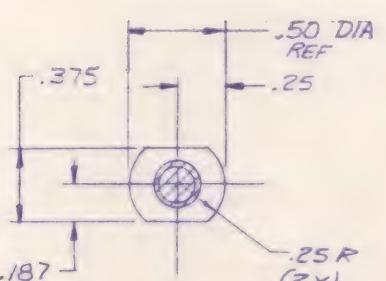
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3	WHT. /BLK.	
4	WHT./ORG.	CO18125
5	BLU.	
6	VIO.	
7	WHT./RED	
8	GRN.	
9	BLK	CO19056
10	BRN.	CO19056
11	RED	CO19056
12	N/C	N/C
13	YEL.	
14	WHT./GRN.	CO18125
15	ORG.	



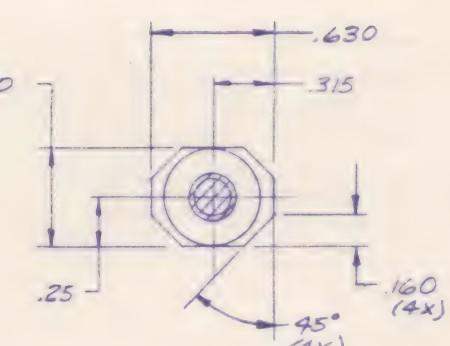
DETAIL C
SCALE NONE
TYPICAL 14 PLACE



SECTION F-F

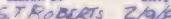


SECTION G-G



SECTION II-II

SEE SHEETS 2&3 FOR APPLICABLE NOTES AND SPECS.
NOTE: * SH 2&3 ARE 'A' SIZE

018988	CX5200	UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ON ANGLES ± .01° SURFACE FINISH ✓ xx x .01 xxx x .005	DO NOT SCALE DRAWING DRAWN BY S. T. ROBERTS DATE 2/9/82	 Atari, Inc. 1265 Borregas Avenue Sunnyvale, Calif. 94088 A Warner Communications Company
WORK ASSY	USED ON	MATERIAL:	TITLE: CONTROLLER CABLE ASSEMBLY 14 CONDUCTOR MOLDED	
APPLICATION		SEE NOTES SH 2	  PROJECT: CONTROLLER CABLE DRAWN BY J. Vaughan 3-8-82 MFG. INSTRUCTIONS	
		SEE NOTES SH 2	SIZE E DRAWING NO CA018145	REV 9

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REV	REVISION DATE	ISSUE	APPROVAL
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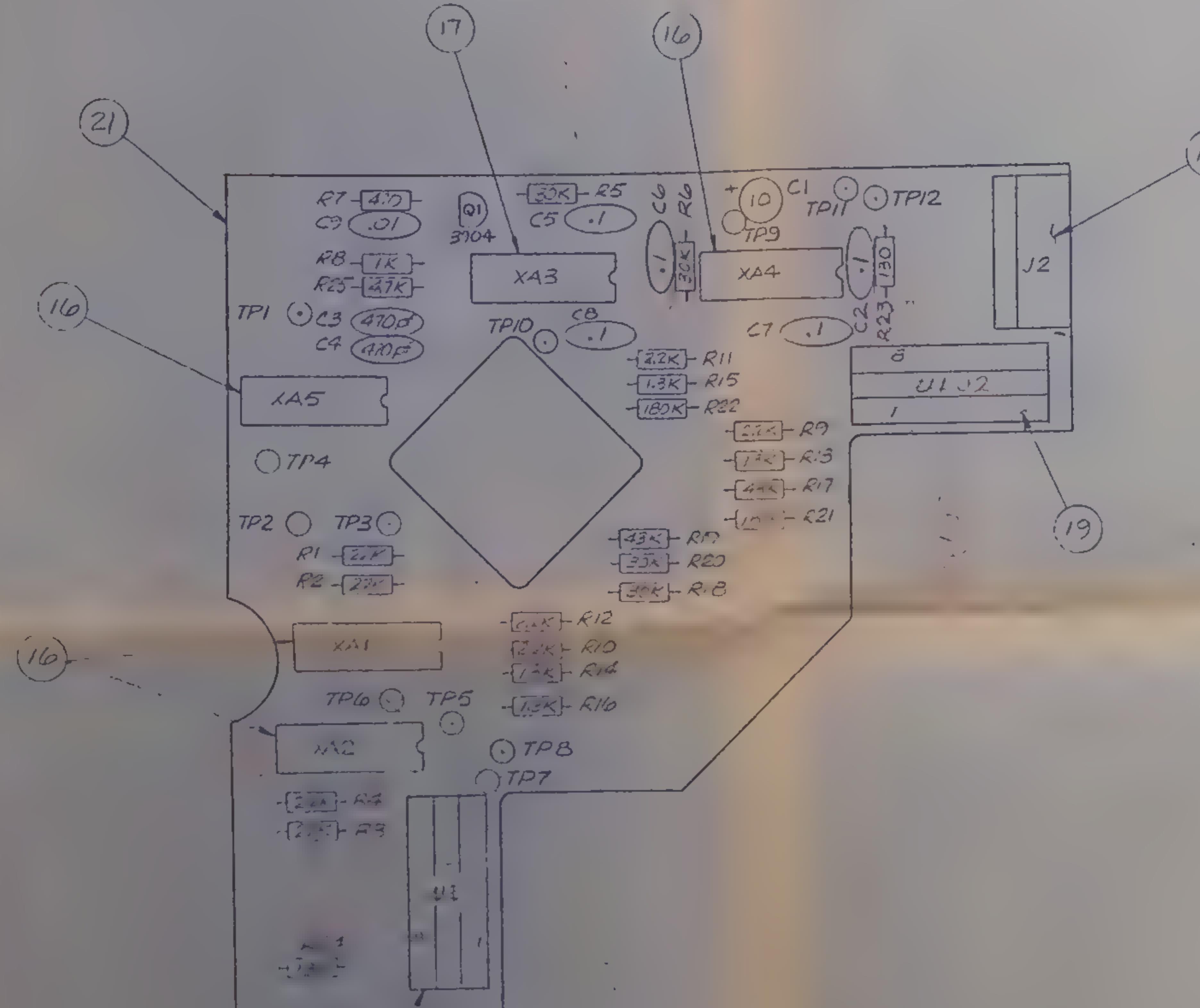
D

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C

B



LINES UNLESS OTHERWISE SPECIFIED

1. ALL LENGTHS ARE IN MILLIMETERS.

2. ALL DIMENSIONS ARE IN MM.

REVISED FOR LATEST CHANGES

Dk 1/2

LATEST REVISION

LAST USED	NOTES
C9	
R25	
A5	
U2	
J2	
C1	
XA5	

ATARI, INC.	1272 Borregas Avenue Sunnyvale, Calif. 94089	ATARI
CRESTWOOD	FACE SLEEVES	CRESTWOOD
D	CHIPS	D

B

NOTES: UNLESS OTHERWISE SPECIFIED

1. ALL RESISTOR VALUES ARE IN OHMS, 1/4W 5%.
2. ALL CAPACITORS ARE IN UF.

A



REVISED FOR LATEST CHANGES

OK 11/22/82

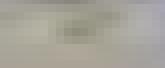
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NOV 11 1982

LATEST REVISION

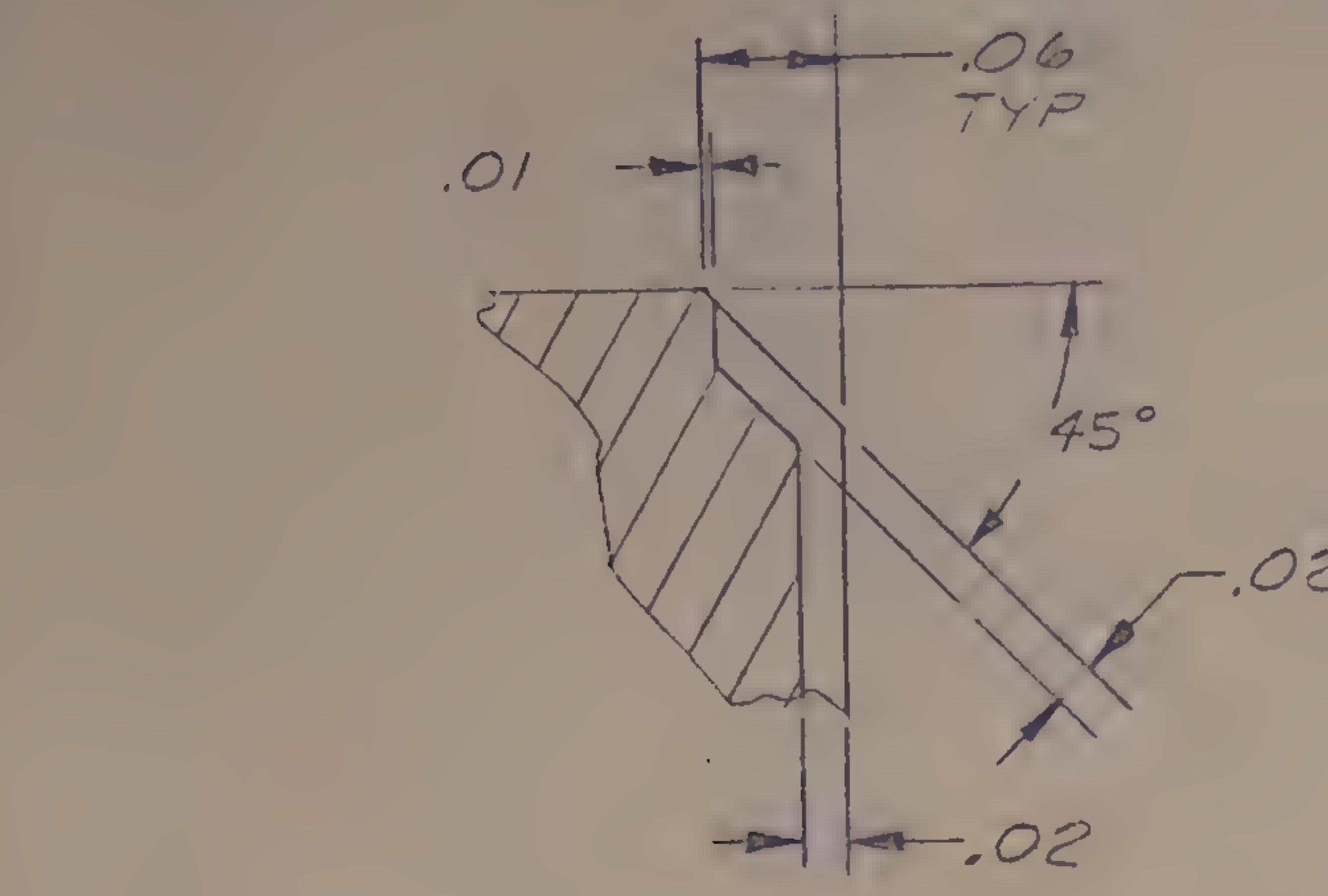
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R25	
A5	
U2	
J2	J1
Q1	
XA5	

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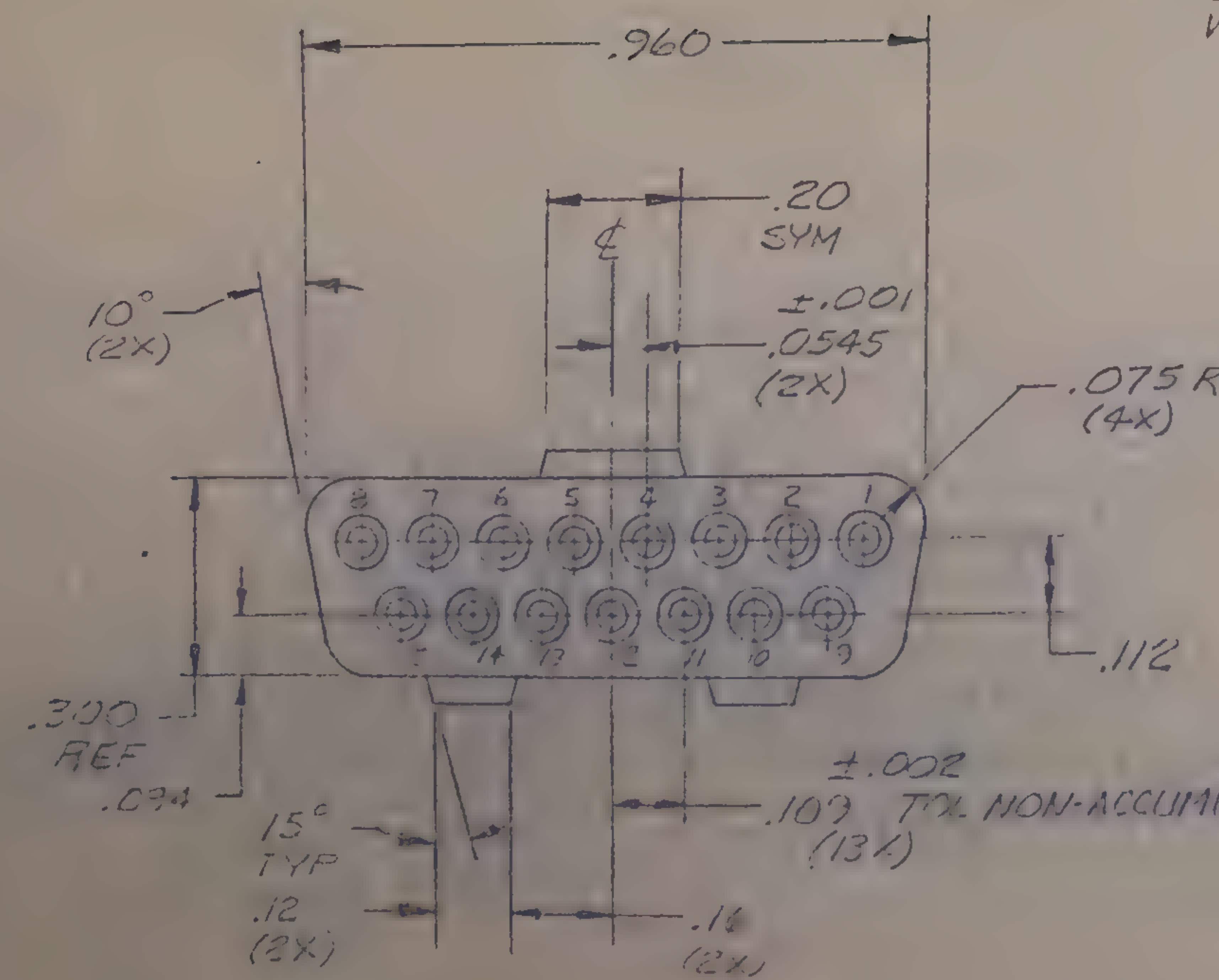
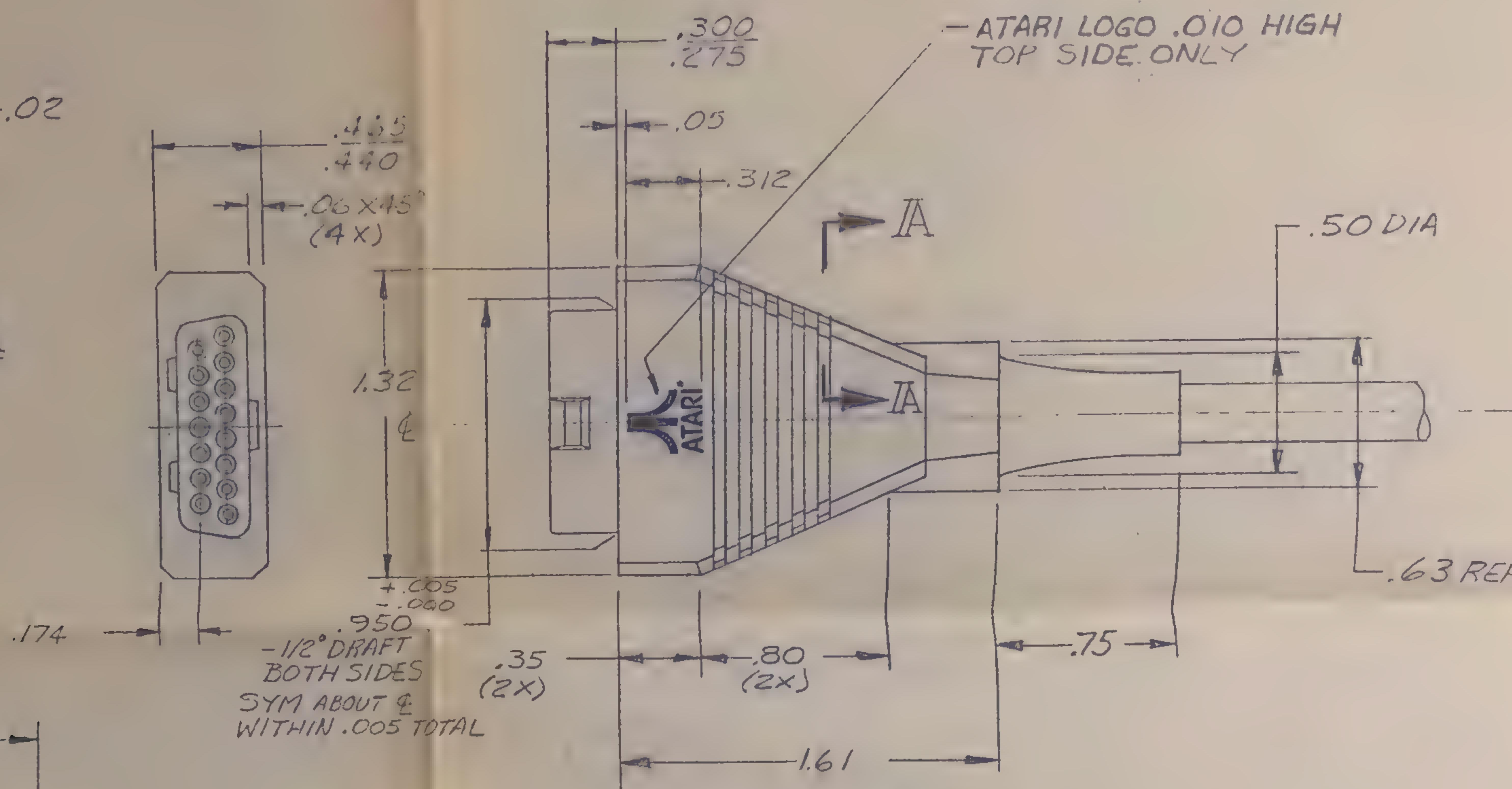
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APPLICATION		$.xx = \pm .03$	
		$.xxx = \pm .005$	
MATERIAL:		ENGINEER	DATE
		J. Hooper	10/6/62
FINISH:		ENGINEERING MGR.	DATE
		R. C. White	
QUALITY ASSISTANT		DATE	
		R. C. White	
DRAWING NO.		D	CAD20141
SCALE		2X	
Atari, Inc. 1272 Borregas Avenue Sunnyvale, Calif. 94086			
 ATARI  A.C.			
CX55 TRAKBALL			
PC-B SUB-ASSY (POWER)			

**FOR APPLICABLE NOTES AND SPECS.
SH 2&3 ARE 'A' SIZE**

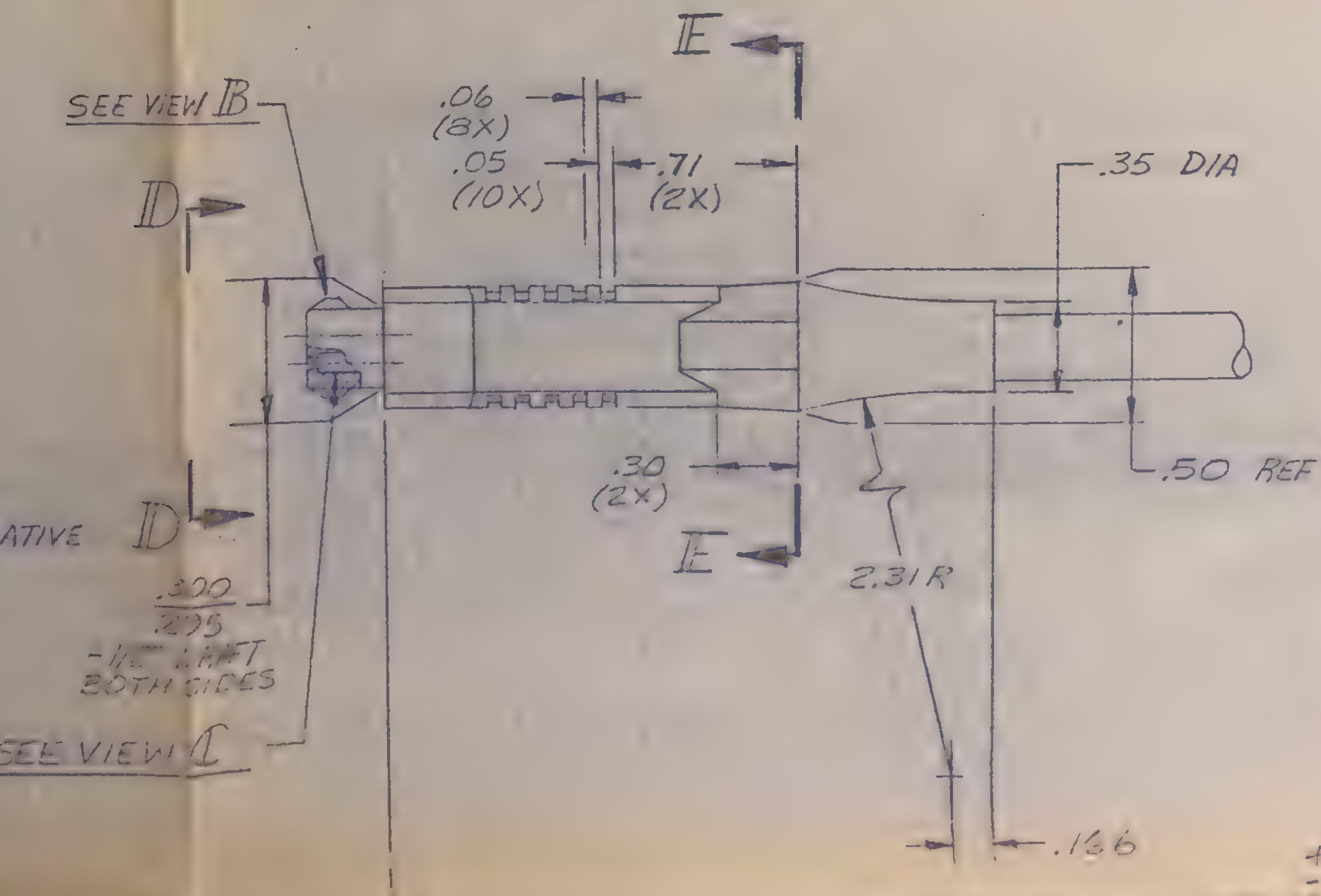
MAR 21982 MAR 2 1982
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SECTION A-A



VIEW D-D



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7	CELESTA WTS 250/250	1,2	100

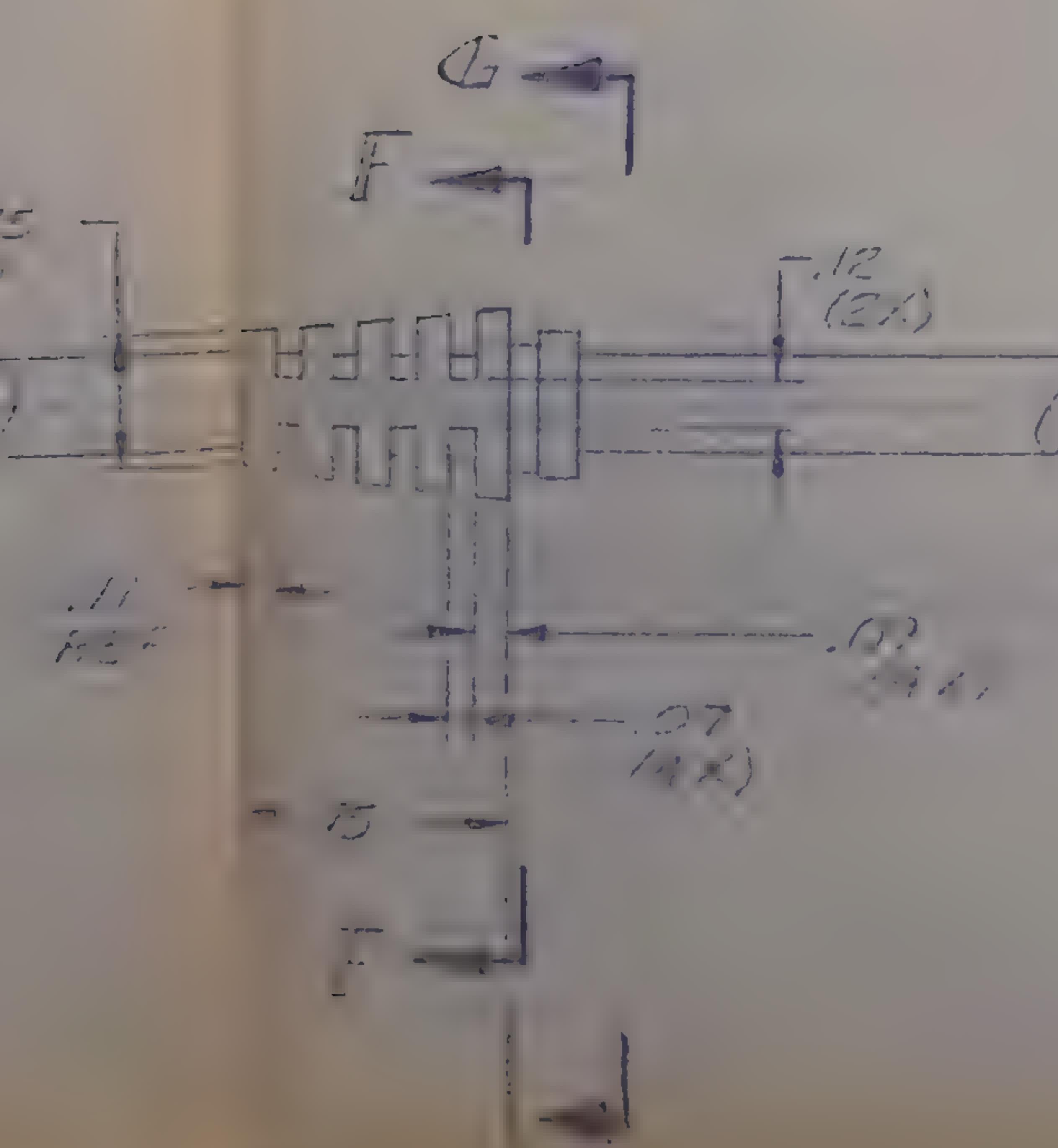
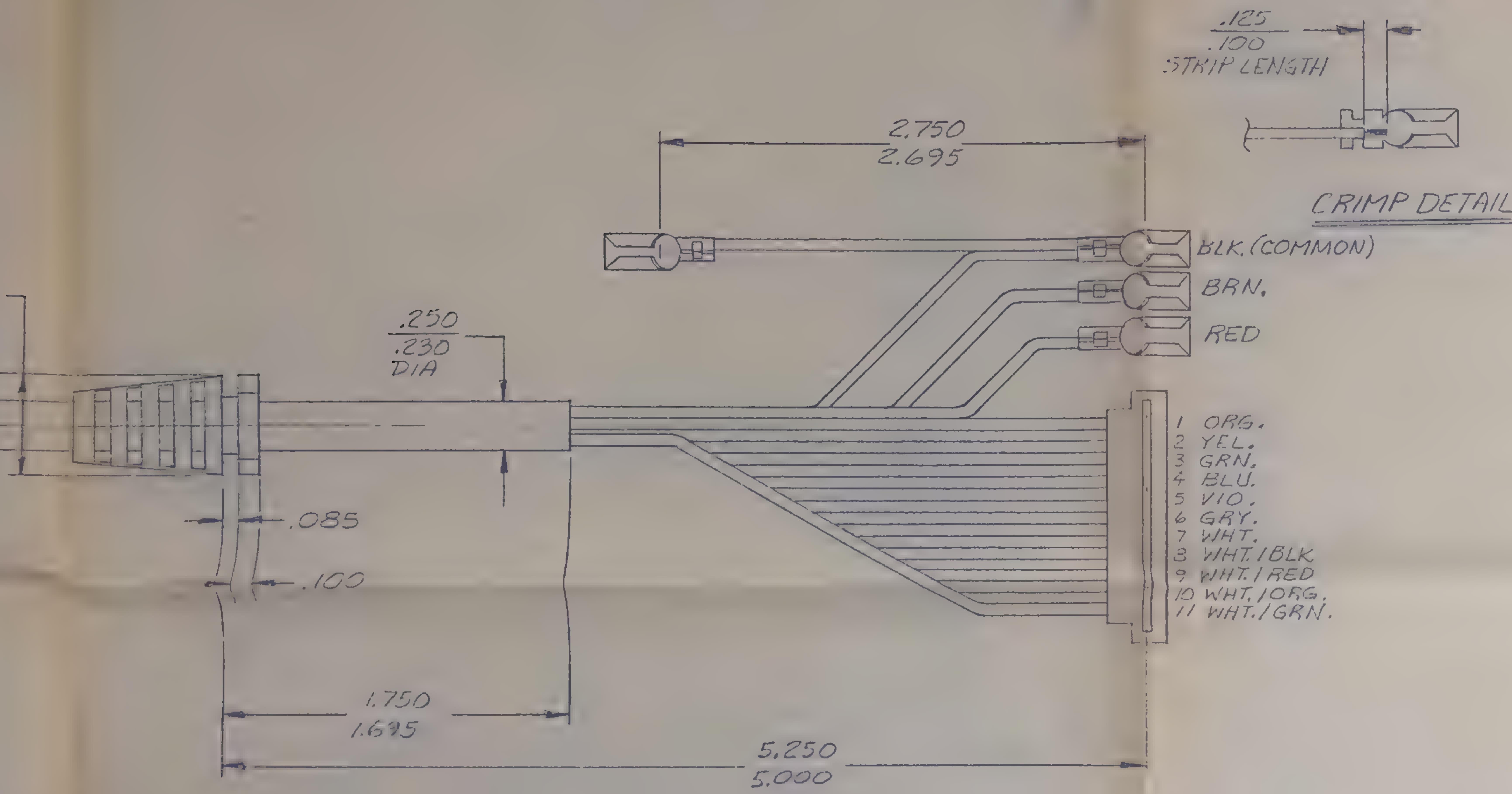
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145-18010 NOVEMBER 1961

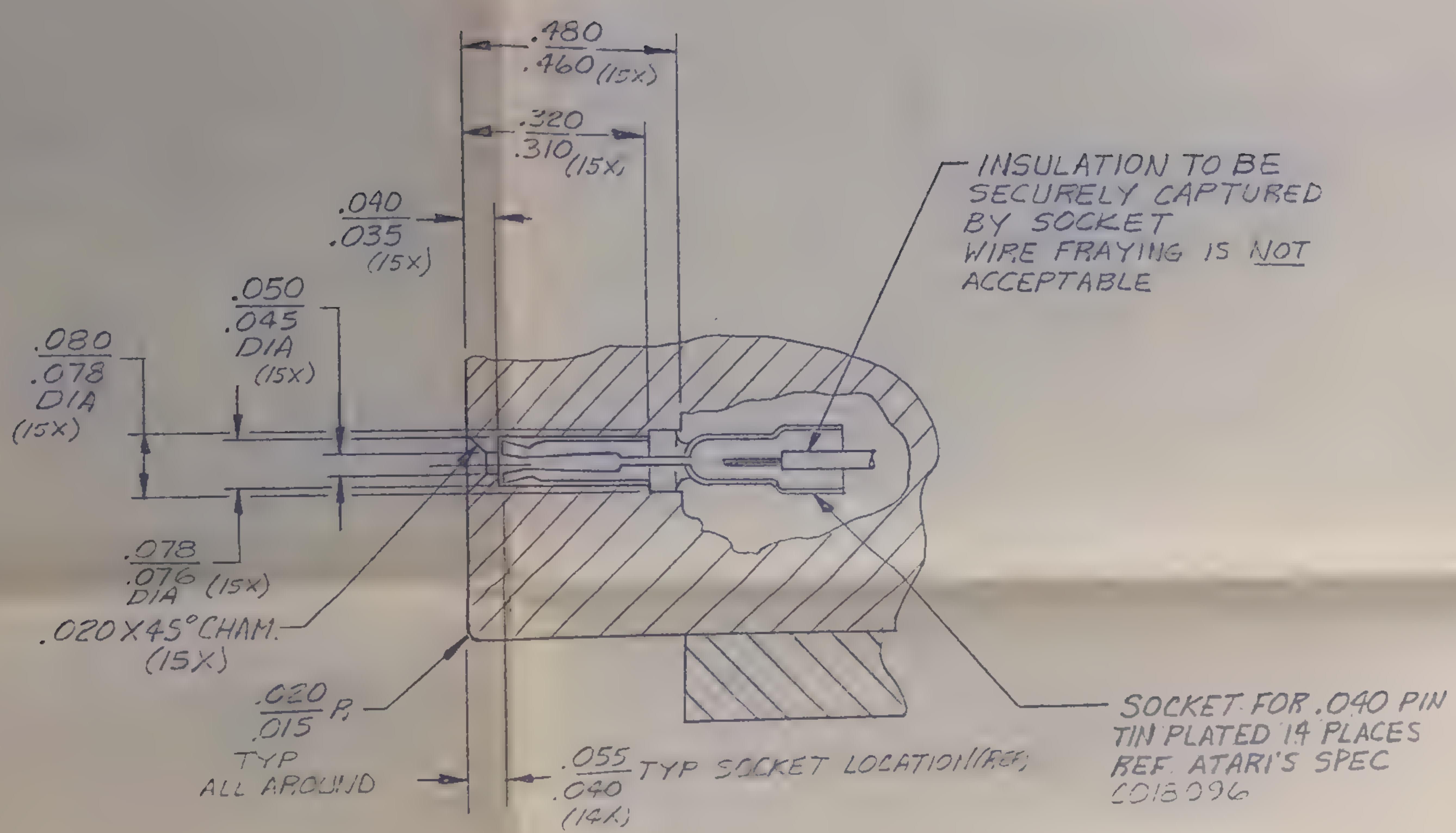
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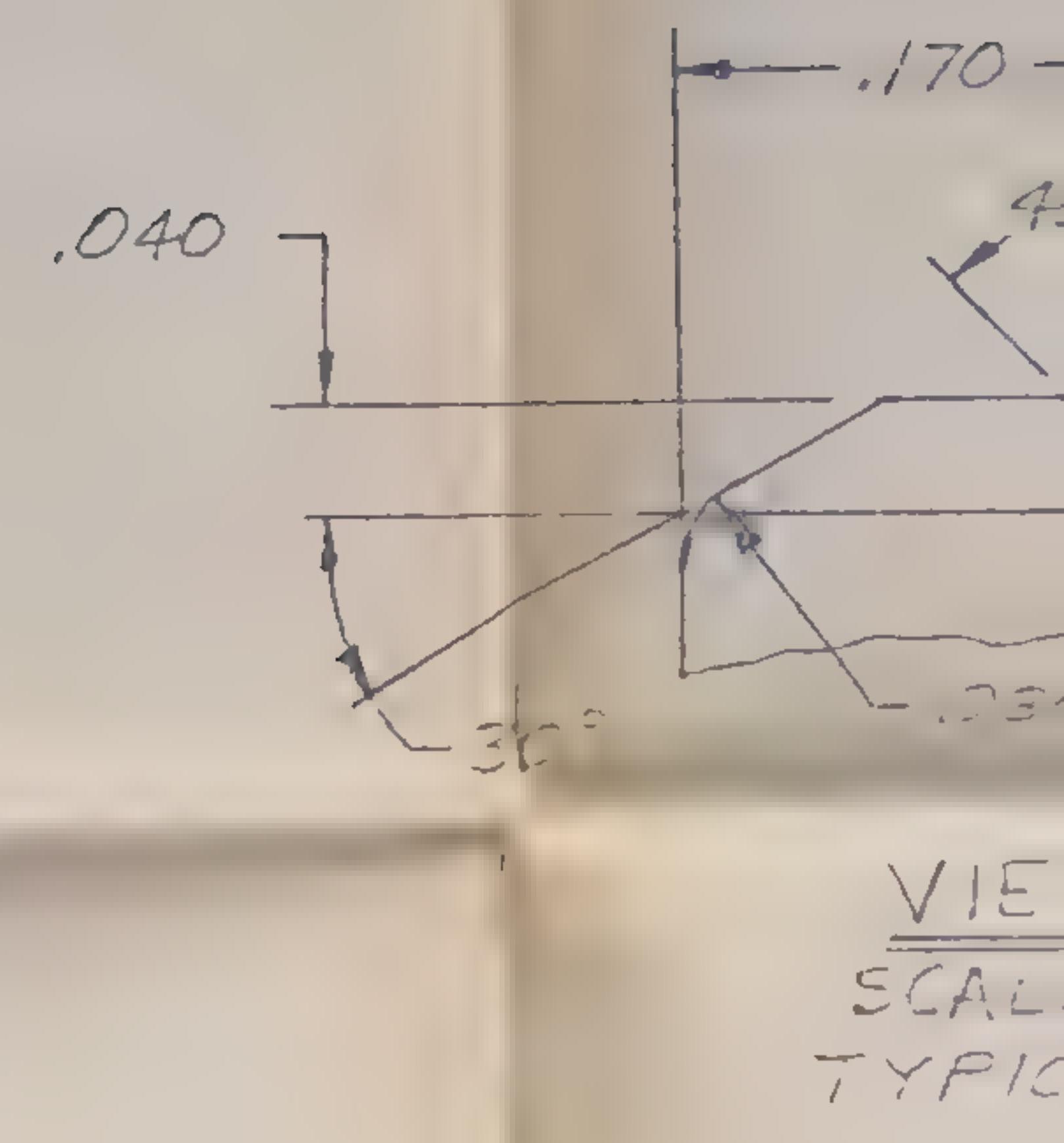
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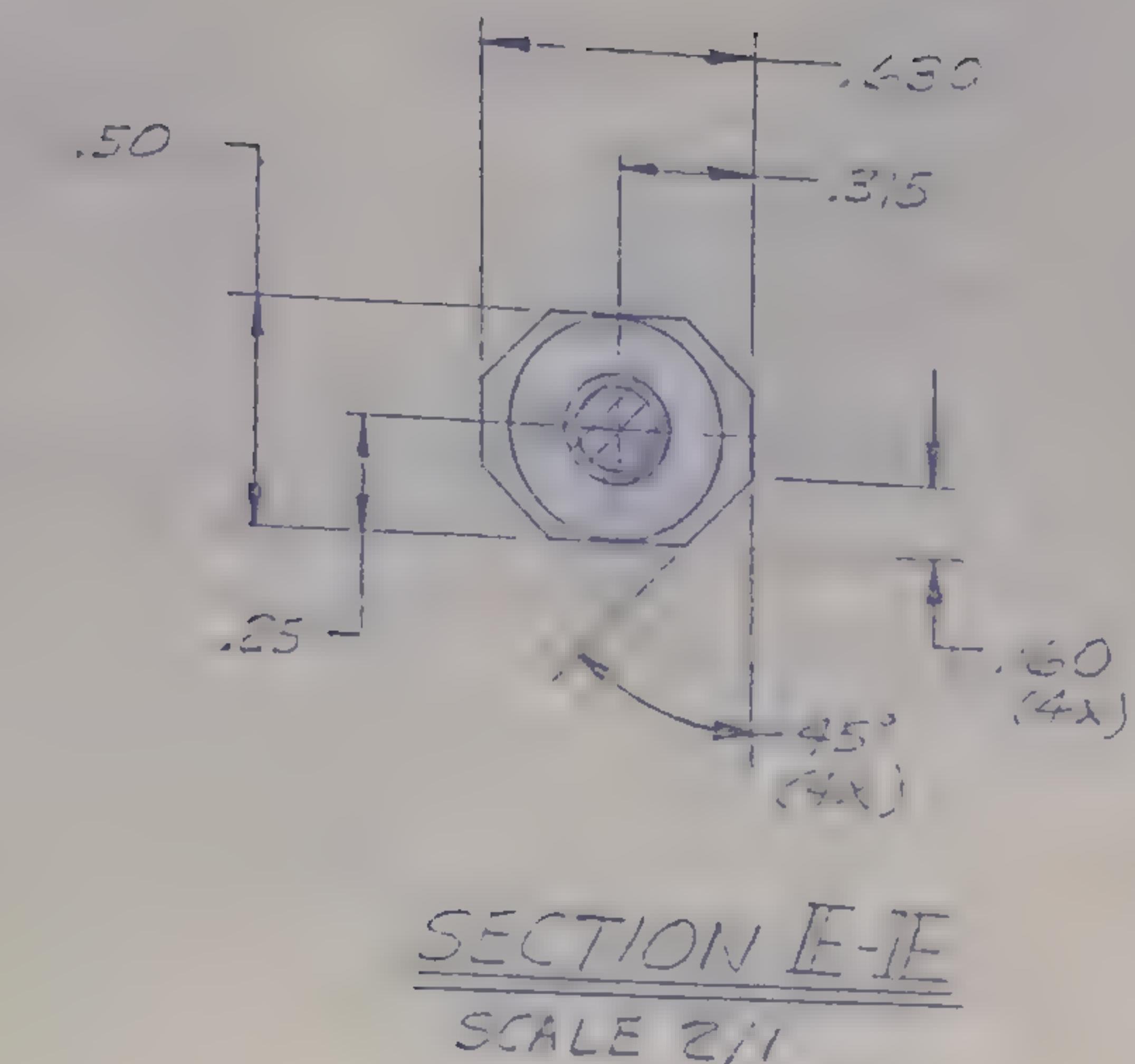
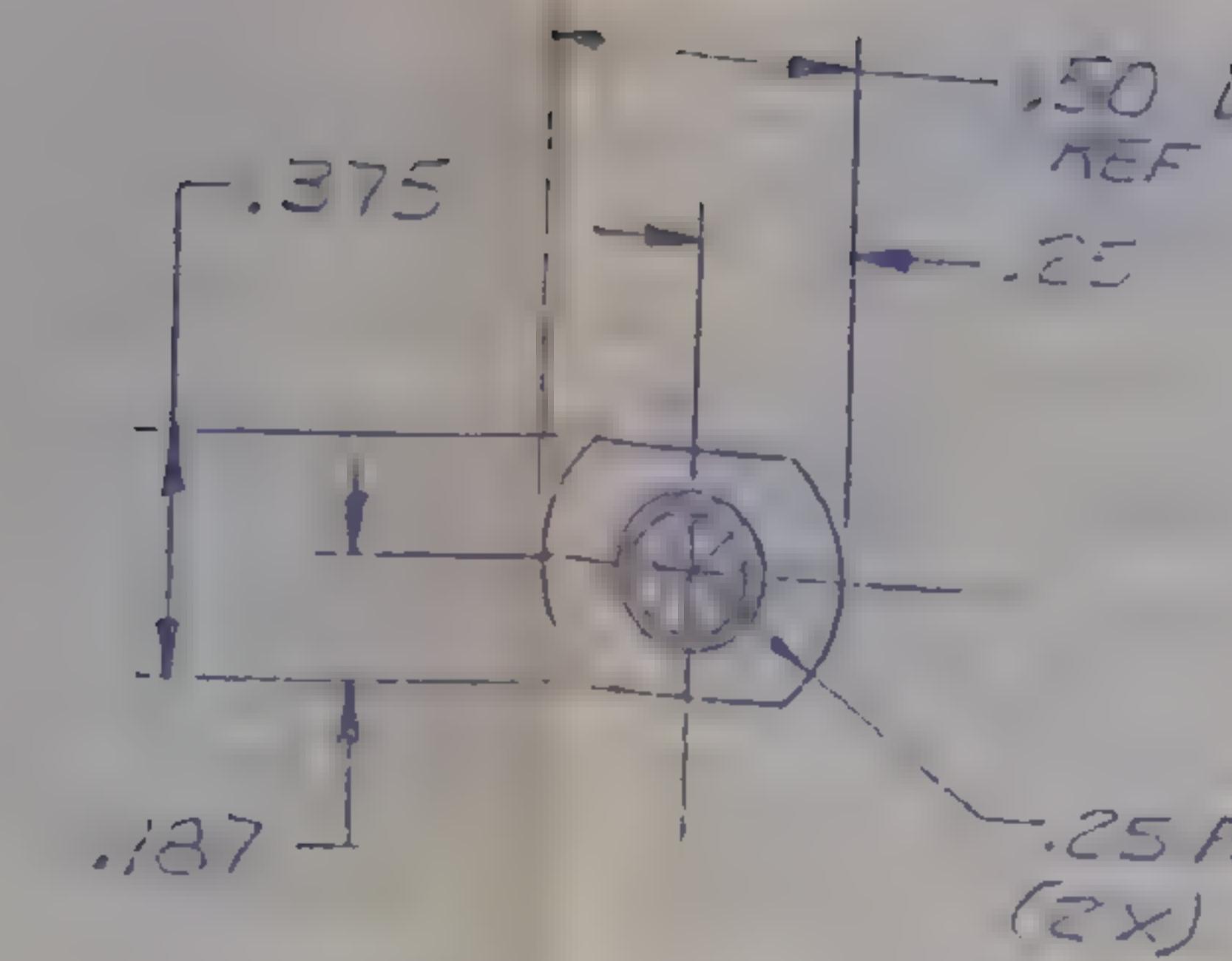
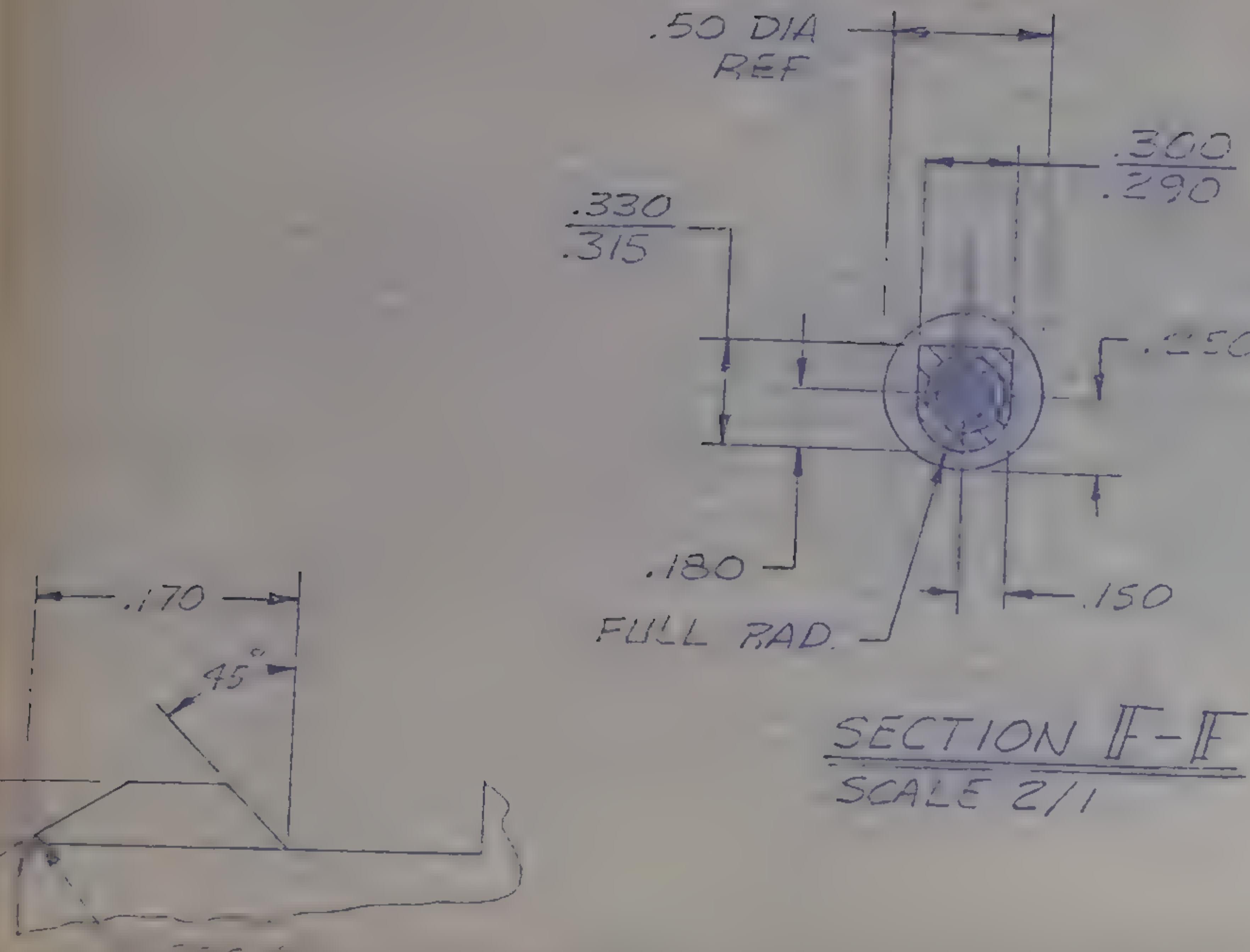


CONNECTOR COLOR CODE	
PIN	WIRE COLOR
1	GRY.
2	WHT.
3	WHT./BLK.
4	WHT./ORG.
5	BLU.
6	VIO.
7	WHT./RED
8	GRN.
9	BLK.
10	BRN.
11	RED.
12	N/C
13	YEL.
14	WHT./GRN.
15	ORG.



DETAIL C
SCALE NONE
TYPICAL 14 PLACES





SEE SHEETS 2&3 FOR APPLICABLE NOTES AND SPECS.
NOTE: * SH 2&3 ARE 'A' SIZE

MAR 21 1985 MAR 21 1985

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UNITS OF MEASURE USED ALL DIMENSIONS ARE IN INCHES ANALYSIS - A-10 SIGHTED ✓ REVISIONS ✓	DO NOT SCALE DRAWING DRAWN BY Date APPROVED BY Date	Atari Inc. 1215 Bernasas Avenue San Jose, Calif. 95132
MANUFACTURER DATE ATARIO REV E	PROJECT ENGINEER MFG ENGINEER	TITLE CONTROLLER CABLE ASSEMBLY 14 CONDUCTOR MOLDED
SEE NOTES REV E	SHEET E DRAWING NO CA018143	SCALE SHEET

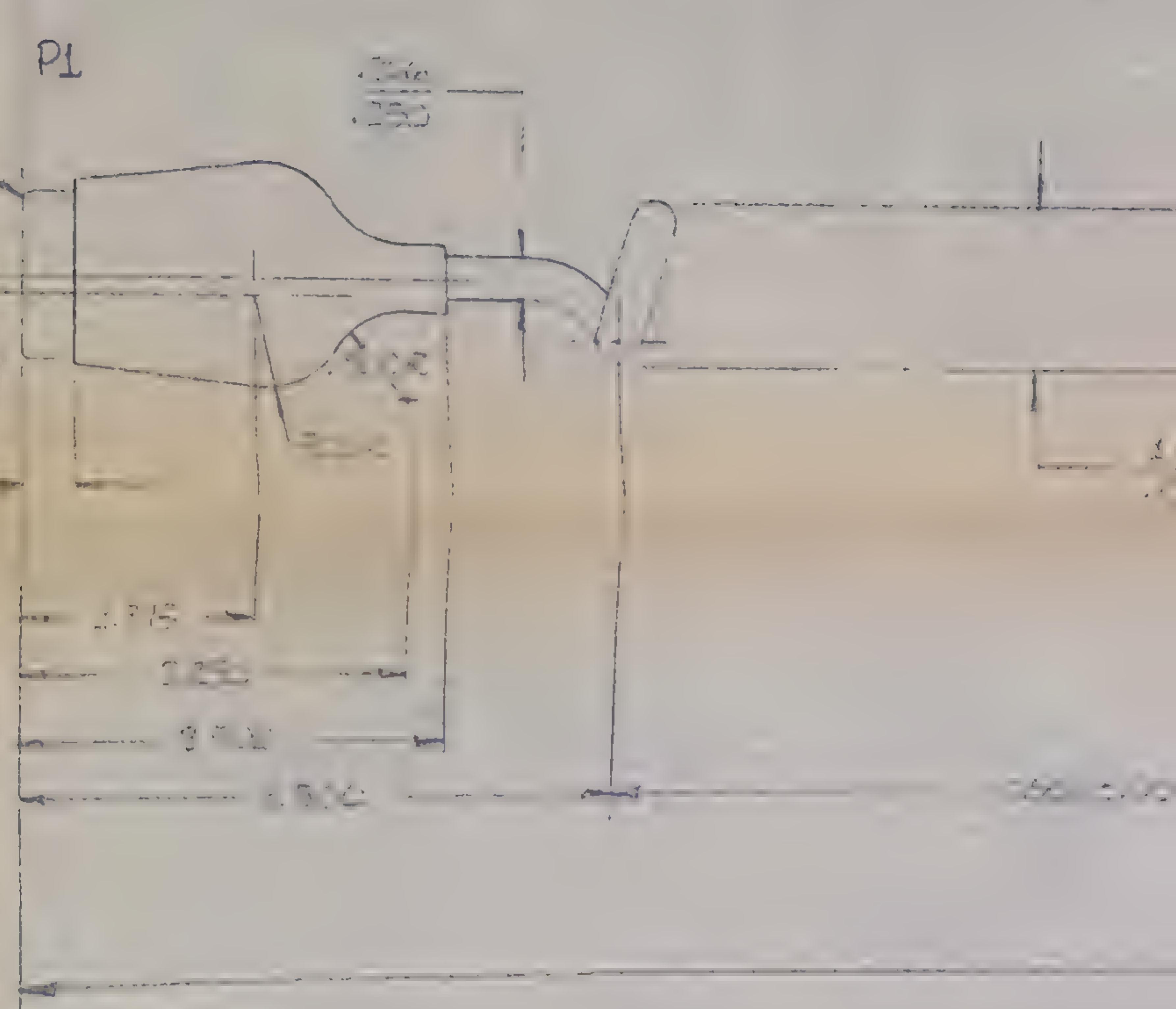
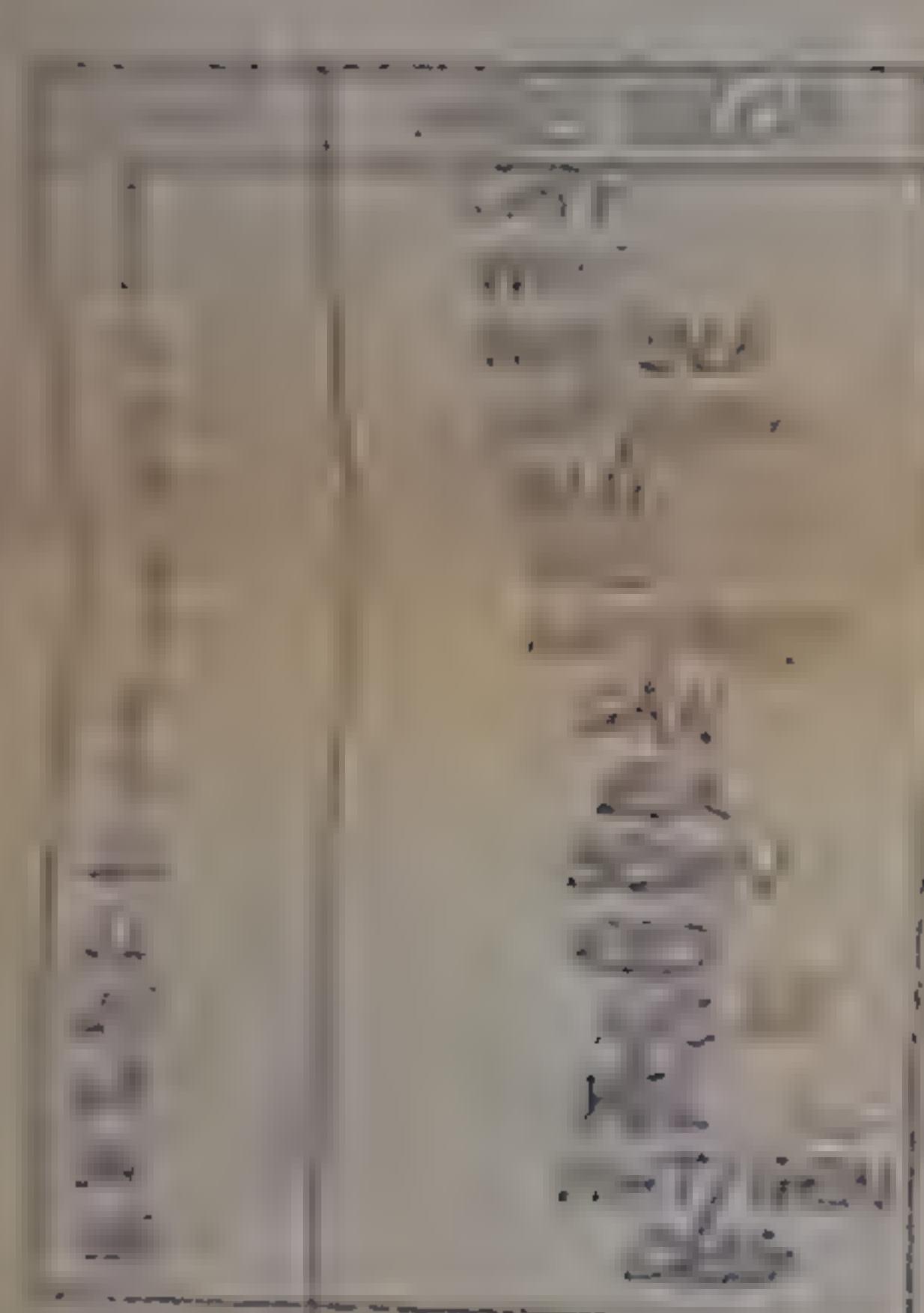
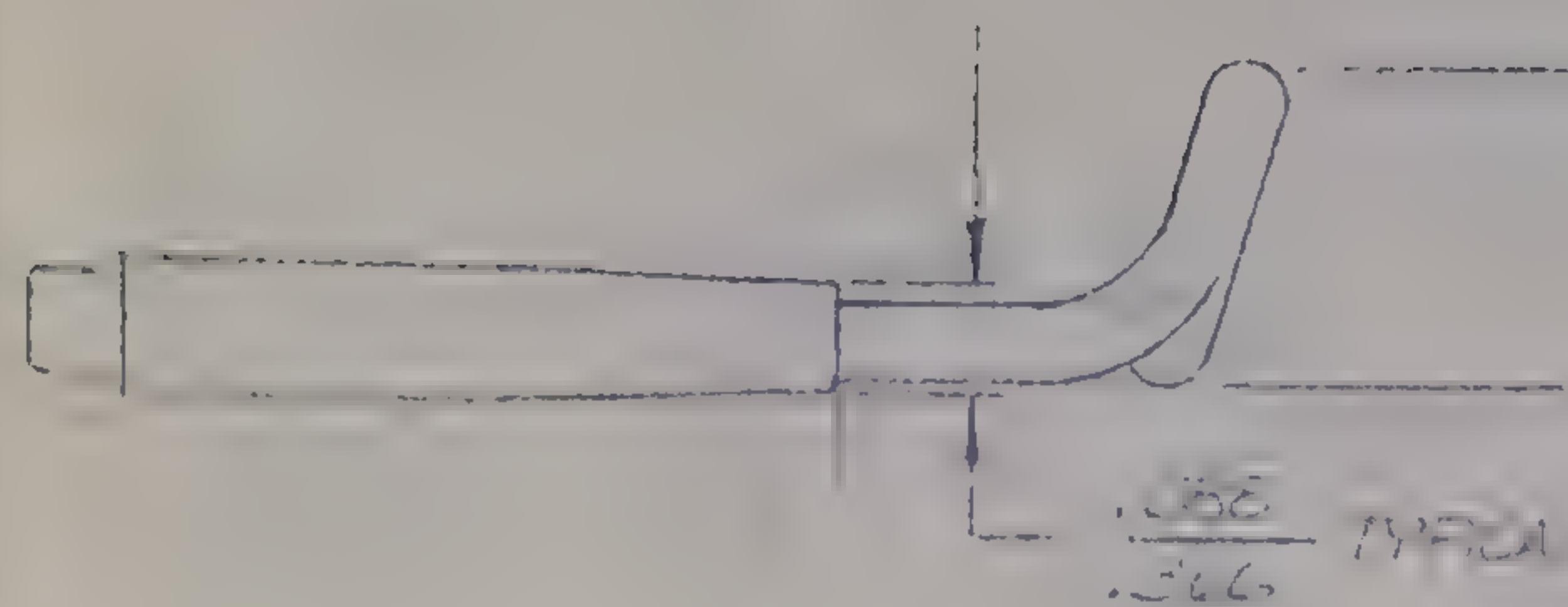
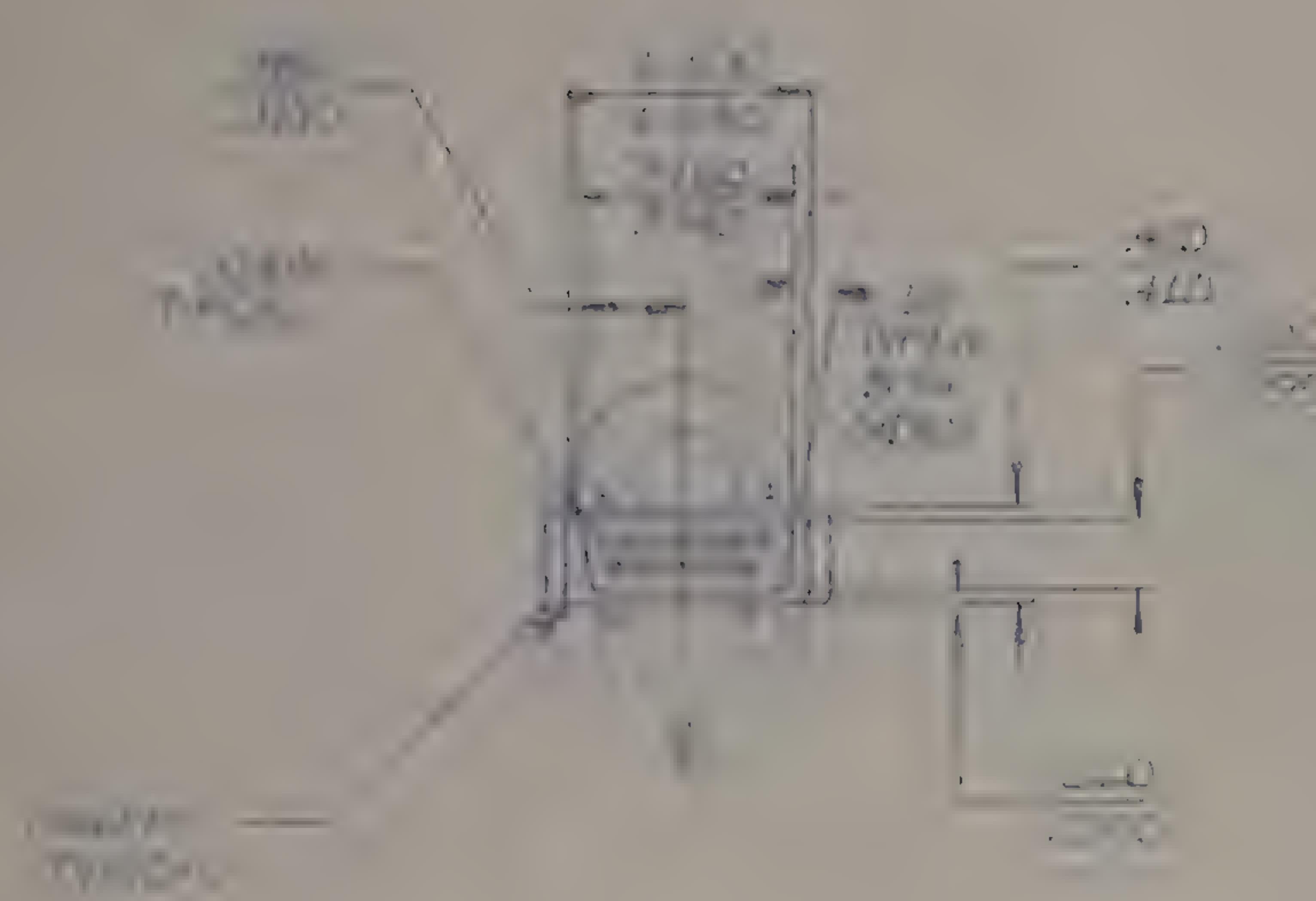
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MAY 12, 1900
CLARK COUNTY, WASH.
WILLIAM A. COOPER,
CITY CLERK.
G. F. DODDINGHAM, CLERK
W. H. COOPER, CLERK.

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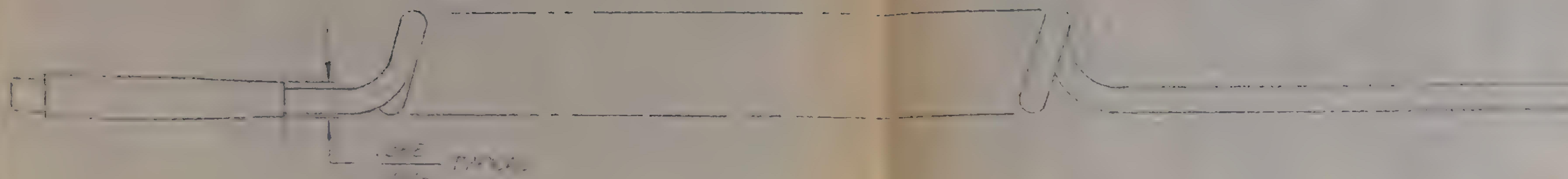
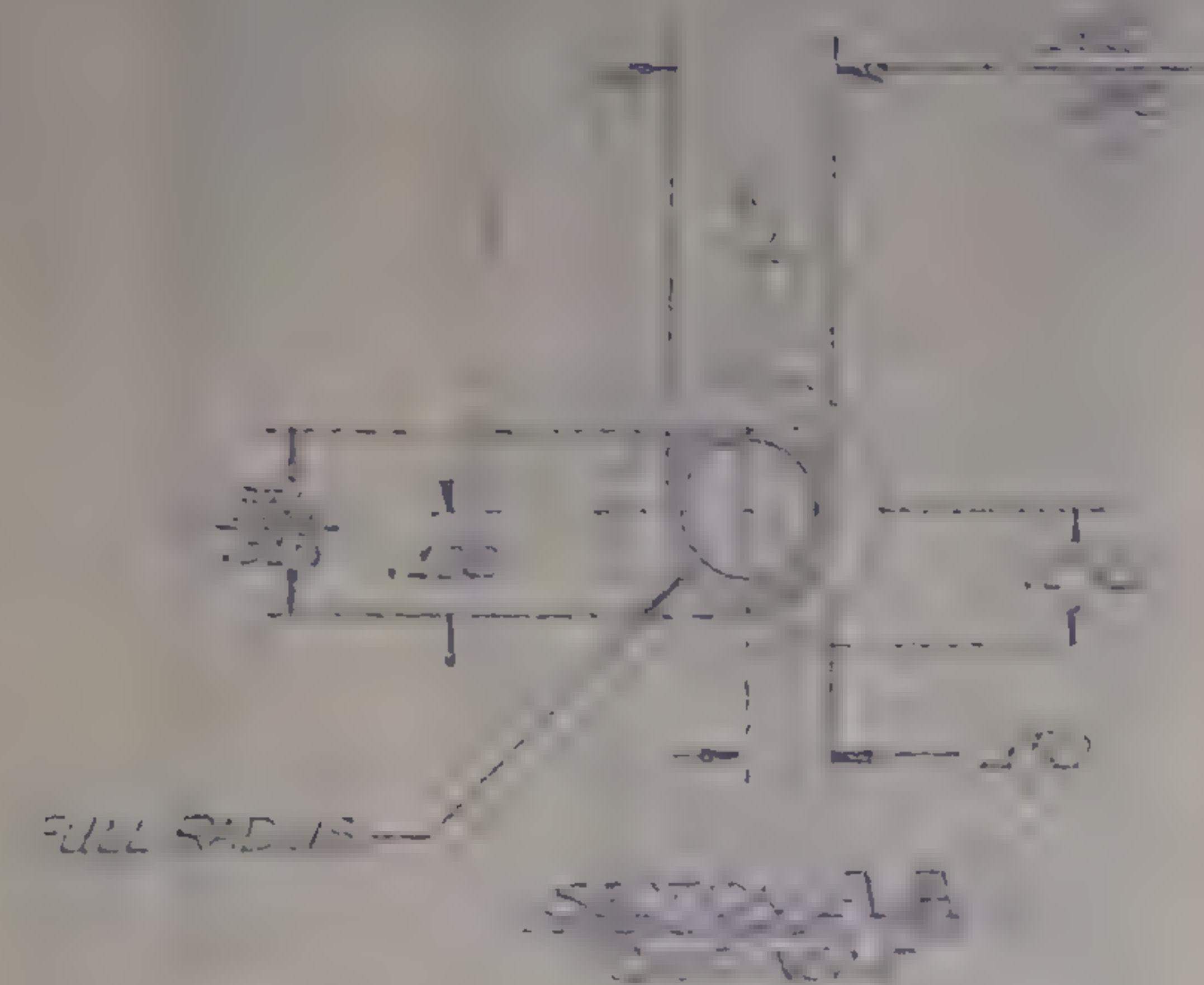
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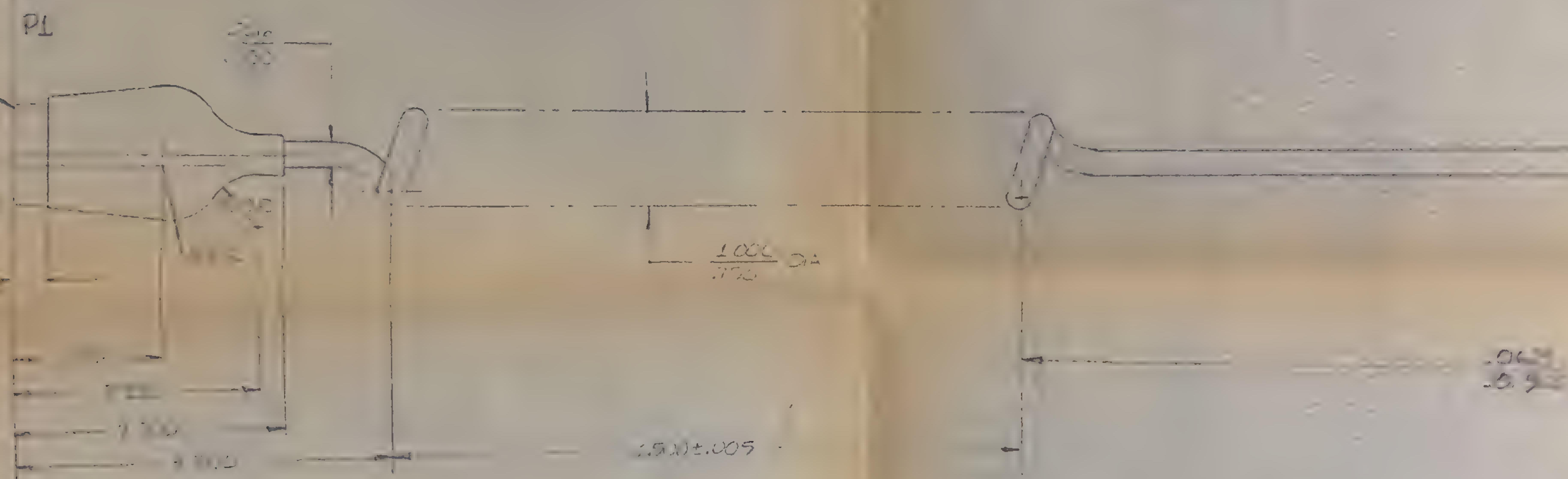
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P1



120.0 (800)
MAX. EXPANSION AT 100° C. INCH.
NO MAX. EXPANSION AT 0°F. (31.6°C.)
RETROFIT TOOL LENGTH AFTER 100° C. EXPANSION
TO 140.0 FT, 27.00 INCHES, SEE ANGLES & LENGTH.

~ PRELIM
FOR INFORMATION
ONLY

PART		NEXT ASSY	USED ON	APPLICATION	MATERIAL
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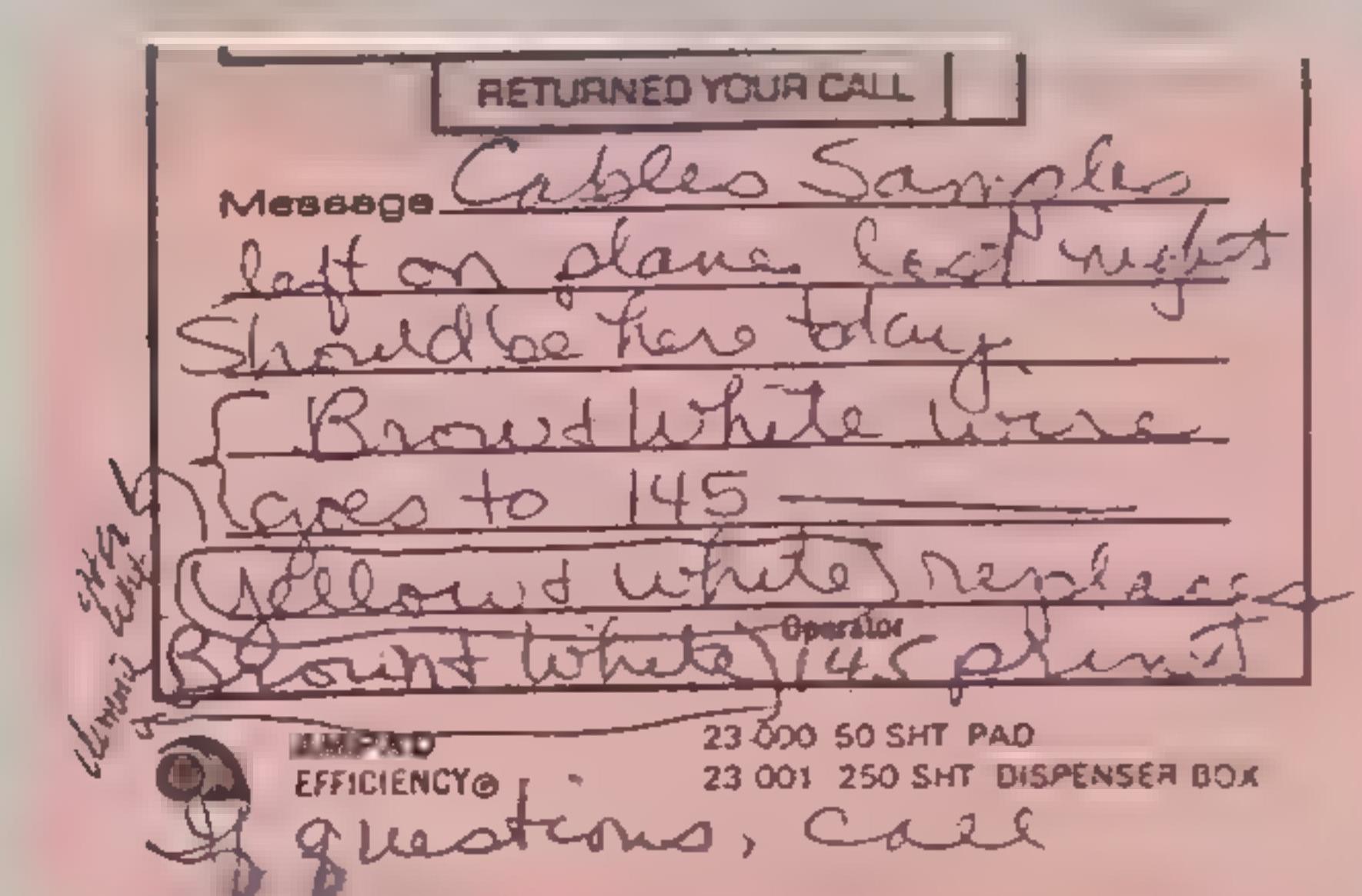
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SYM	REVISIONS DESCRIPTION	DATE	APPROVED
3	REVISIONS: NEW COIL OUTLINE PLUG PINCUT ADDED	4-3-8	

The diagram illustrates a crimp type slide assembly. On the left, a rectangular component labeled 'CRIMP TYPE SLIDE' contains two vertical slots. A horizontal bar, labeled 'SLIDE', extends from the right side of this component. The bar features a central slot and two vertical slots at its ends. A small vertical tab is positioned above the central slot. To the right of the slide, a dashed line indicates its path through a tube or channel. At the far right, a circular component labeled 'STOP' is shown.

~ PRELIMINARY ~

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DEC 14 1981

		UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ON ANGLES ± 10°	
NEXT ASSY PART NO.		DRAWN BY <i>(Signature)</i>	DATE 4-13-21
USED ON		CHECKED	DATE
APPLICATION		ENGINEER	DATE
MATERIAL		ENGINEERING MGR.	DATE
FINISH:		QUALITY ASSURANCE	DATE
MFG. ENGINEERING		MFG. ENGINEERING	DATE
		SHEET	10
		NOTE	
		SCALE	
		DRAWING NO	CONTROLLER CABLE
		SIZE	D
		W	A Warner Communications Company
		ATARI®	1272 Borregas Avenue Sunnyvale, Calif. 94086
		Atari, Inc.	

KYNARTM Piezo Film

A unique, flexible polymer film,
with high piezo and pyroelectric activity.





KYNAR™ Piezo Film—A versatile new transducer material

Piezoelectric materials, which transform a mechanical force to an electrical response and conversely, transform an electrical signal to a mechanical motion, have been known for many years. Examples are highly polar natural crystals and ceramics such as quartz and barium titanate, respectively. These materials are dense, brittle, stiff and difficult to produce in large sizes and impractical to fabricate into complex shapes. Recently, polymeric piezoelectric films have been developed. They are pliant, flexible, tough and lightweight. Of all known polymers, those based on vinylidene fluoride show the highest piezo- and pyroelectric activities. Polyvinylidene fluoride, PVDF, is the base resin used in the development of KYNAR Piezo Film by the Pennwalt Corporation. This specialty film is now available in various thicknesses for application as transducers for many industrial devices.

Molecular structure

Polyvinylidene fluoride, PVDF, is a semi-crystalline high molecular weight polymer of repeat unit ($\text{CH}_2\text{-CF}_2$) whose structure is essentially head-to-tail, i.e. $-\text{CH}_2\text{-CF}_2\text{-}(\text{CH}_2\text{-CF}_2)_n\text{-CH}_2\text{-CF}_2-$. PVDF is approximately 50% crystalline and 50% amorphous. The principal crystalline forms of PVDF are the highly polar β form and the non-polar α form shown in Figure I. High piezo response

is associated with the polar β form in which the hydrogen and fluorine atoms are arranged to give the maximum dipole moment per unit cell. The dipole moments of the crystallites are randomly oriented with respect to each other unless the film is electrically polarized. Pennwalt produces KYNAR Piezo Film by means of carefully controlled processing steps which include mechanical orientation and treatment in an intense

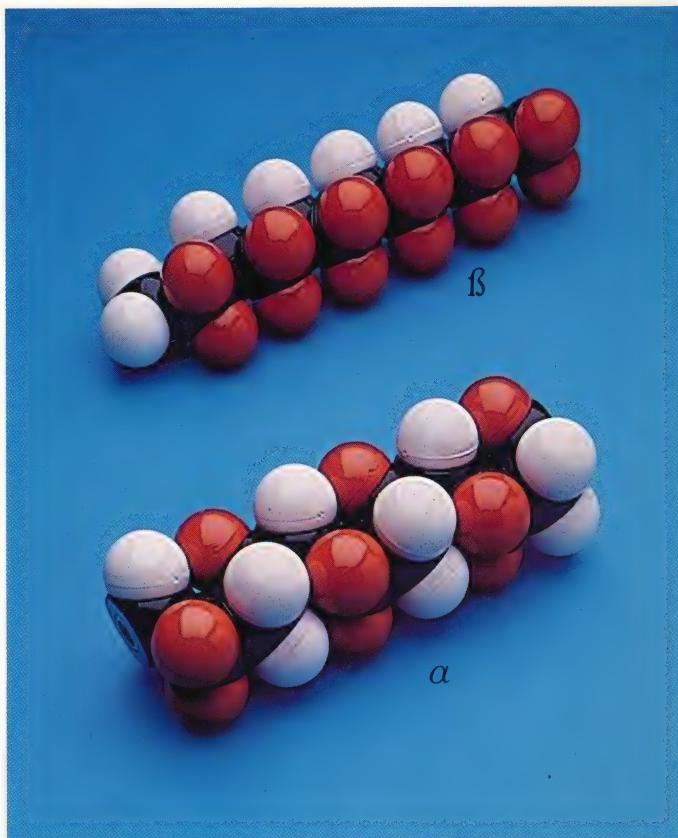


Figure I

electric field. The resulting product containing predominantly oriented β form crystallites exhibits a large net polarization. It is this net polarization that gives the film its high piezoelectric and pyroelectric activities.

KYNAR Piezo Film—Unique Characteristics

The basic characteristics that make KYNAR Piezo Film unique and useful in many electronic transducer applications are:

- High pyroelectric sensitivity.
- High piezoelectric sensitivity in planar, thickness, and hydrostatic modes.
- Good fidelity throughout a broad range of frequencies.
- Low mechanical and acoustic impedance.
- High dielectric strength—much higher than ceramics.
- Resistance to moisture and high humidity.
- Tough, flexible and lightweight.
- Available as thin film—readily cut and shaped to form complex configurations.
- Easily laminated to produce bimorph and multimorph elements which multiply transducer response.
- Not subject to breakage and loss of dipolar properties when subjected to mechanical impact.

Properties of KYNAR Piezo Film
and other Materials (in Length Expansion Mode)

Materials	Cut	Density	Elastic Stiffness	Relative Dielectric Constant	Piezoelectric Constant				Coupling Factor	Acoustic Impedance			
					ρ kg/m^3	c N/m^2	ϵ/ϵ_0	d m/V (coul/N)	e N/V m (coul/m ²)	g V m/N	h V/m		
Quartz	X	(10^3)	(10^9)		2.65	77.2	4.5	(10^{-12})	(10^{-2})	(10^{-3})	(10^7)	(%)	(10^6)
Rochellesalt	45°X	1.77	17.7	350	275	490	90	2	15	50	380	10	14.3
PZT	Z	7.5	83.3	1200	110	920	10	110	90	160	73	73	5.6
BaTi_2O_3	Z	5.7	110	1700	78	860	5.2	5.2	60	21	30	30	30
Kynar Film	Z	1.78	3	12	23	6.9	200	65	12	12	2.5		

KYNAR Piezo Film Properties

The level of piezo activity in KYNAR Piezo Film may be readily determined by standard test methods.

The coordinate system showing the piezo constants, d_{31} , d_{32} , and d_{33} are illustrated in Figure II. The first index (subscript 3 on d_{31}) specifies the electrical (polar) axis. The second index (subscript 1 on d_{31}) indicates the mechanical (stress or strain) axis. These constants along with typical basic properties of KYNAR Piezo Film are listed in Table I.

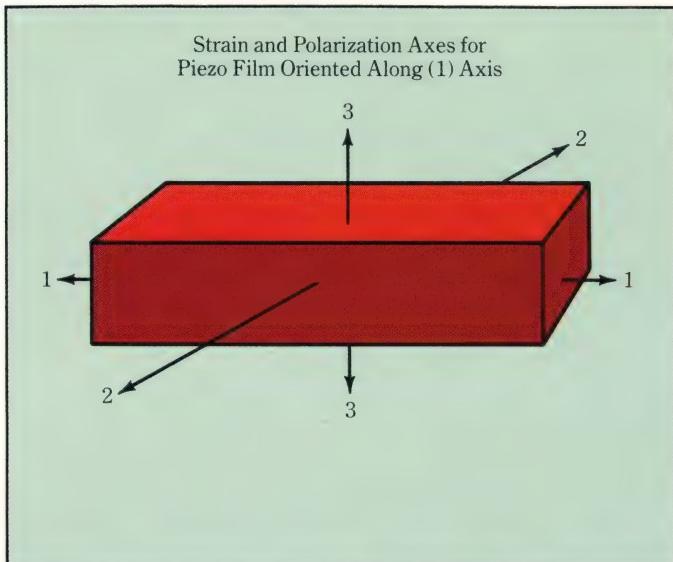


Figure II

The changes in several properties with frequency and temperatures are shown in Figures III through VI on page 3. The thermal stability of piezo activity as shown in Figure III demonstrates that after an initial decay, piezo activity becomes very stable. Most of the decay below 100°C is caused by thermally induced mechanical relaxation and is not related to depolarization effects.

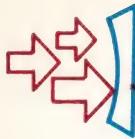


Figure IV illustrates the dependence of dielectric permittivity and dissipation factor on frequency at ambient temperature. As a result of its relatively low dielectric permittivity (100 fold less than piezo ceramics), the g-constants (voltage output coefficients) of PVDF are significantly greater than those of ceramics. Thus PVDF can be made into very responsive sensors of mechanical signals.

The relationships between electrical impedance and frequency for various thicknesses of KYNAR Piezo Film, 100 sq. cm in area, are shown in Figure V. These data are important for matching film impedance to associated components in the circuit. The influence of frequency on the electro-mechanical coupling factor "k₃₁" is shown in Figure VI. Although k₃₁ and therefore the efficiency of energy transfer is low compared to ceramic transducers, KYNAR Piezo Film elements can be used at much higher fields than ceramics which result in desirable mechanical deflections. For example, because its dielectric strength is 70 times that of PZT ceramics, the maximum input capability for electrical energy of PVDF is 40 times greater and the corresponding output of mechanical energy is 5 times greater.

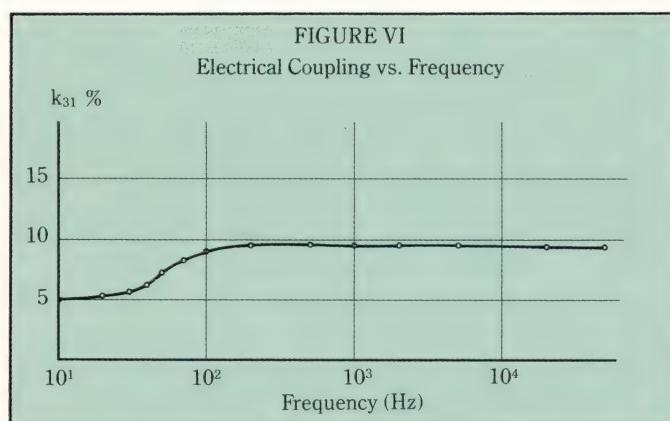
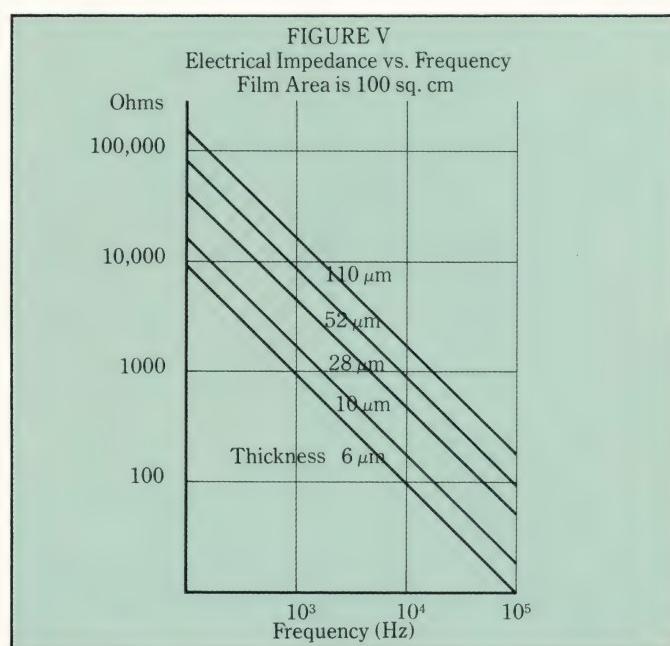
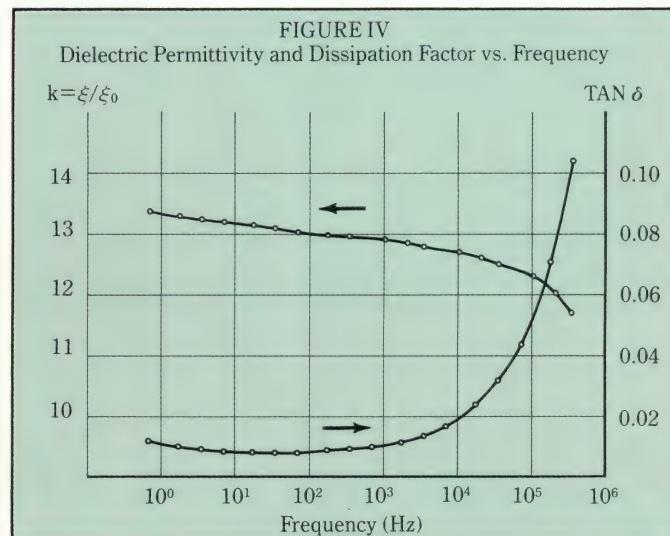
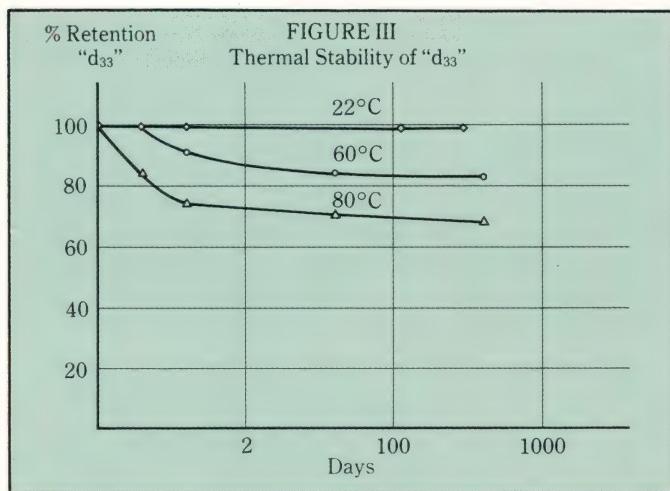


TABLE I
TYPICAL PROPERTIES OF KYNAR PIEZO FILM

PROPERTY		VALUE	UNITS
Thickness		6-125	μm
Surface Conductivity of Metallized Film	A1	1-4	$\Omega \square^{-1}$
	Ni	10-25	
Static Piezoelectric Strain Constant	d_{31}	20-25	$\text{pCN}^{-1} (\text{pmV}^{-1})$
	d_{33}^*	20-22	
Static Voltage Output Coefficient	g_{31}	0.230	VmN^{-1}
	g_{33}	0.210	
Electromechanical Coupling Factor	k_{31}	9-15	% at 100 Hz
Pyroelectric Coefficient	p	23-27	$\mu\text{Cm}^{-2}\text{°K}^{-1}$
Shrinkage in Machine Direction	60°C	2	% after annealing 100 hrs.
	80°C	4	
Relative Dielectric Permittivity	ϵ/ϵ_0	12 ± 1	at 1000 Hz
Dielectric Loss Factor	$\tan \delta$	0.015-0.02	at 1000 Hz
Volume Resistivity	ρ	10^{13}	Ωm
Tensile Strength at Yield	MD**	—	10^6Nm^{-2}
	TD**	40-110	
Tensile Strength at Break	MD	160-330	10^6Nm^{-2}
	TD	30-55	
Elongation at Break	MD	25-40	%
	TD	380-430	
Young's Modulus of Elasticity = Elastic Stiffness = c_E	MD	1.5-3	10^9Nm^{-2}
	TD	1.1-2.4	
Melting Point		165-180	°C
Flammability, LOI		44	%O ₂
Thermal Conductivity		0.13	$\text{Wm}^{-1}\text{°K}^{-1}$
Specific Heat		2.5	$\text{MJm}^{-3}\text{°K}^{-1}$
Density		1.8	g(cm)^{-3}
Thermal Expansion Coefficient		1.4	10^{-4}°K^{-1}
Sound Velocity***		1.5-2.2	kms^{-1}

*measurements were made in hydraulic press (e_{33}/c_{33}) **MD = Machine Direction (1) and TD = Transverse Direction to film orientation (2)
***longitudinal and thickness modes.

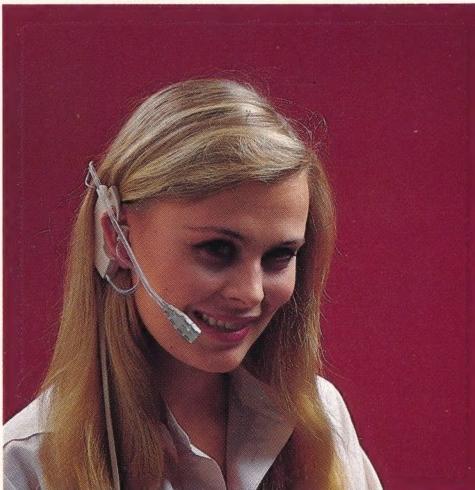


Audio Applications: as the active element in microphones and stereo pickups, and in speakers and headphones, KYNAR Piezo Film affords lightweight, compact design, easy formability to desired geometry, and high fidelity response. It has low acoustic and mechanical impedance and is well-suited for the design of noise-cancelling microphones.

Switching Components: as patterned switch elements in "finger-pressure touch action" keyboards and key pads for typewriters, telephones and computer terminals, KYNAR Piezo Film has virtually unlimited

life. Such switches have been tested for millions of operations without failure. These elements are also useful in impact detectors, coin sensing systems, and actuators for explosives.

Instrumentation: as sensors for instruments used to monitor vibration, deformation, acceleration, pressure, fluid flow, and seismic pulses. In medical applications as sensors for monitoring heartbeat, breathing, and blood flow.



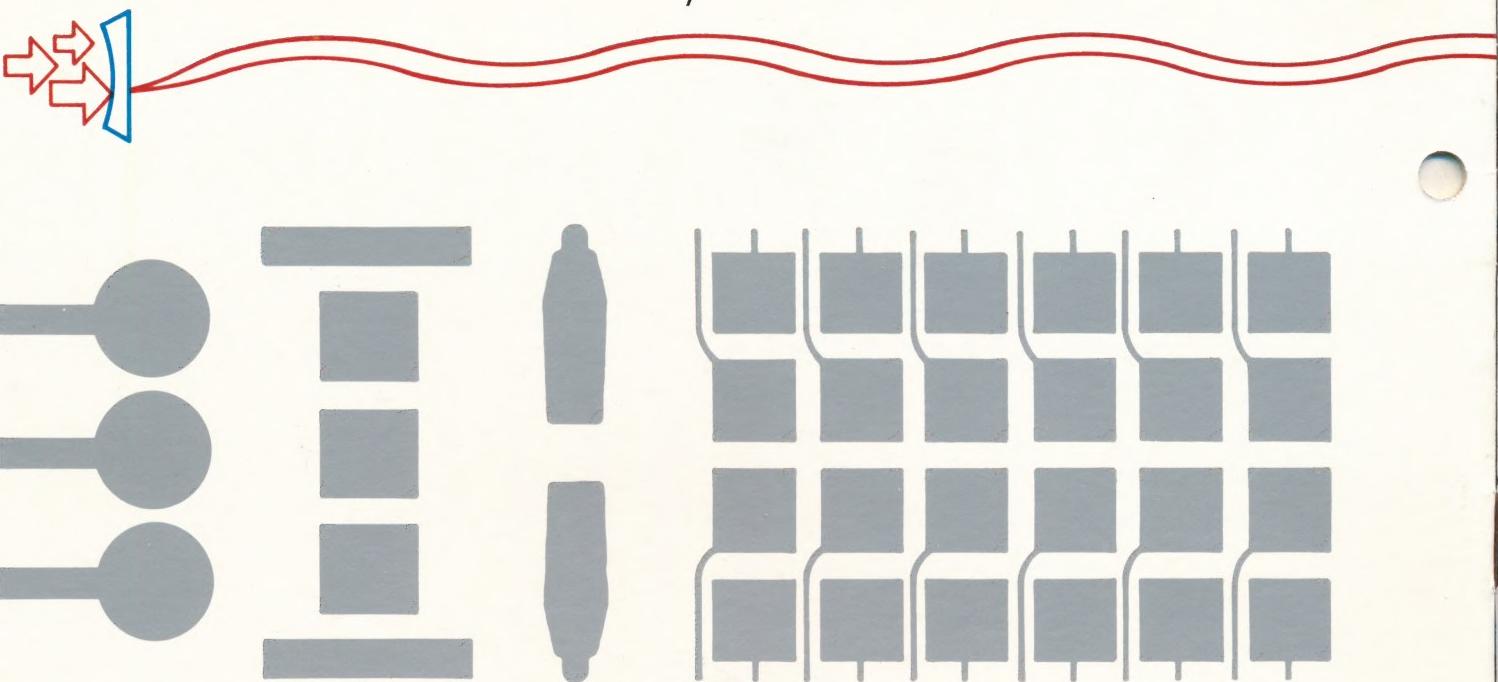
Ultrasonic Sensing: because its acoustic impedance is close to that of water and body tissue, KYNAR Piezo Film is an excellent choice for applications in medical imaging equipment. It is also being evaluated for non-destructive testing instruments and for range-finding systems.

Underwater Sound Detection: as large, flexible elements for hydrophones, sonobuoys and towed arrays used for submarine detection and oil exploration.

Heat sensors: because of its excellent electrical response to incident infra-red radiation, KYNAR Piezo Film is used in intrusion and fire alarms, heat scanners, and pyroelectric energy control systems. It also shows promise for applications in infra-red imaging equipment and electrostatic copying.

Flexure-mode Transducers: as bimorph constructions in motion displays, "motorless" fans, pumps, shutters and position sensors.





Film Thickness

KYNAR Piezo Film can be supplied in a range of thicknesses, from a few microns to several hundred microns.

Thin films are recommended where a high efficiency of conversion of electrical signals into mechanical motion is needed as in headphones, speakers, and bimorph designs utilizing the d_{31} mode. Thin film is also preferred for pyroelectric applications where rapid response is required.

Thick films are recommended in applications where a voltage is generated by thickness change or hydrostatic pressure. An example is sonar transducers for under-water sound detection.

Bimorph Elements

KYNAR Piezo Film is readily laminated into bimorph stacks, which increase the mechanical motion generated in cantilever devices. Either series or parallel arrangements can be used. This technique is also applicable to sensors as a means of multiplying electrical output.

KYNAR Piezo Film is available in the following forms and styles:

- Continuous rolls
- Sheets
- Various thicknesses
- Unmetallized and metallized surfaces
- Custom-metallized patterns (above)
- Specialized elements to customer specifications

Pennwalt is supplying KYNAR Piezo Film and customized elements to companies throughout the world for use in commercially available products as well as for many new products under development.

For further information and technical service contact the KYNAR Piezo Group, Pennwalt Corporation, 900 First Avenue, P.O. Box C, King of Prussia, PA 19406-0018, (215) 337-6750 or call toll free (800) 345-8112; in Pennsylvania, (800) 662-2444.

KYNAR™ PIEZO FILM

KYNAR™ Piezo Film brings you a combination of characteristics never before available: a flexible film with the highest piezoelectric and pyroelectric activity of any polymer, available in large sheet sizes, easy to form into complex shapes, and free of the limitations of

fragile, brittle and hard-to-fabricate crystals and ceramics.



No wonder KYNAR Piezo Film is being used successfully in applications such as these:

Audio applications. Microphones, headphones, speakers. KYNAR Piezo Film has low acoustic and mechanical impedance, and frequency response from DC to GHz.

Switches. Keyboards and keypads for typewriters, telephones, computer terminals. High resistance to impact and fatigue means film won't shatter or deform over millions of touch operations.

Industrial and Medical Instrumentation. As sensors for pressure, vibration, strain and fluid flow. Medical equipment: for ultrasonic imaging, for monitoring of

heartbeat, and measuring respiration and blood flow.

Underwater Sound Detection.

As elements for hydrophones and sonobuoys. Acoustic impedance is close to that of water.

Heat sensors. For fire and intrusion alarms and for energy control systems.

Motion Devices. For displays, shutters, position sensors, "motorless" fans.

KYNAR Piezo Film is available in commercial quantities, in a range of thicknesses, sizes, and types of metallization



to meet designers' needs. For technical data, price and delivery information, and assistance in customized applications, call toll-free (800) 345-8112, in Pennsylvania, (800) 662-2444, or write to:

KYNAR Piezo Group, Pennwalt Corporation, 900 First Avenue, P.O. Box C, King of Prussia, PA 19406-0018.



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